

DIGBY WELLS  
ENVIRONMENTAL

---

## Kriel Power Station Ash Dump Extension

### Geochemistry and Waste Classification Assessment

---

**Project Number:**

ESK2840

**Prepared for:**

Eskom Holdings SOC Limited

Feb 2017

---

Digby Wells and Associates (South Africa) (Pty) Ltd  
(Subsidiary of Digby Wells & Associates (Pty) Ltd). Co. Reg. No. 2010/008577/07. Fern Isle, Section 10, 359  
Pretoria Ave Randburg Private Bag X10046, Randburg, 2125, South Africa  
Tel: +27 11 789 9495, Fax: +27 11 789 9498, info@digbywells.com, www.digbywells.com

Directors: AR Wilke, DJ Otto, GB Beringer, LF Koeslag, AJ Reynolds (Chairman) (British)\*, J Leaver\*, GE  
Trusler (C.E.O)  
\*Non-Executive

---



This document has been prepared by Digby Wells Environmental.

<b>Report Type:</b>	<b>Geochemistry and Waste Classification Assessment</b>
<b>Project Name:</b>	<b>Kriel Power Station Ash Dump Extension</b>
<b>Project Code:</b>	<b>ESK2840</b>

<b>Name</b>	<b>Responsibility</b>	<b>Signature</b>	<b>Date</b>
Bridget Moeketsi	Field work and reporting		September 2014
André van Coller	Hydro-geochemistry and reporting		October 2014
Lucas Smith	Review		December 2014

*This report is provided solely for the purposes set out in it and may not, in whole or in part, be used for any other purpose without Digby Wells Environmental prior written consent.*

## EXECUTIVE SUMMARY

Digby Wells Environmental (Digby Wells) was tasked to perform a geochemistry and waste classification assessment for the proposed Kriel power station dump extension project. Kriel Power Station is located approximately 6 km northeast of Matla Coal Mine in the Mpumalanga Province (Appendix A, Plan 1). The existing ash dam at the Kriel Power Station is reaching full capacity and Eskom therefore requires the construction of a new ash dam in order to continue operations. If required, and during ongoing construction of the new ash dam, Eskom plans to transfer ash to the neighbouring Matla Power Station and/or increase the height of the existing facility at Kriel Power Station.

The objectives of the study are as follow:

- Geochemically assess the existing ash dam material, as well as fresh ash material to assist with waste classification of the material; and
- Waste classification and liner requirements.

The geochemistry and waste classification project forms part of the bigger hydrogeological investigation. Throughout the process the source term – pathway –receptor methodology was applied to have a holistic understanding of the study area and potential risks to the environment and their significance. The geochemistry and waste classification part of the project serves the sole purpose of characterising the source of potential contamination with the geohydrological study investigating the pathways and receptors.

The following paragraphs summarises the findings of the study:

### **Geochemistry**

The ABA and NAG tests performed on the ash samples allowed for an evaluation of any potential for acid generation from the material analysed or alternatively whether the material is neutralising or not.. The test ABA and NAG results (given in Appendix B) can be summarised as follows:

- All samples have a paste pH of above 11 which is well above the acid producing margin of pH 5. This shows that the material is highly alkaline with a buffering potential. The high pH can however lead to dissolution and higher aqueous activity of metals like Al and B;
- Although pyrite content was observed the total sulphur concentrations in all samples are below the recommended 0.3% and no oxidation of sulphide minerals should lead to acid formation;
- The Neutralising Potential Ratio (AP:NP) is well above 4:1 indicating that the nett neutralising capacity of the material is much higher than any potential for acid production;

- Along with the high NPR, all samples show no NAG potential (all values are less than 0.01) and thus all the ash samples can be classified as non-acid generating; and
- Although no acid generation is predicted there is still a potential for certain elements to leach at high pH levels.

Distilled water tests were performed on two fresh ash slurry samples (ASS3 and ASS2), three ash samples from the existing ash dumps (AEDS1, AEDS2 and AEDS3) and one fly ash sample (FAS1), before being mixed with process water to produce slurry.

The tests on the existing ash dump samples and fly ash samples were to assess and compare the potential changes in material behaviour under normal neutral leaching conditions. The following conclusions have been reached from the results presented in Table 4-5:

- The two fresh samples submitted for testing according to NEM:WA guidelines showed the best leachate quality results with all parameters of concern below the SANS drinking water guideline values, with the exception of pH;
- Both samples showed leachable pH levels above 10 indicating, as mentioned in the mineralogical and ABA interpretations, a high buffering capacity;
- The fly ash and existing ash dump samples however showed leachable concentrations of B, Ba, Cr, Mo and TDS above the recommended limits for drinking water but within the limits of the LCT for waste classification;
- The higher leachability in these samples can be due to the fresh ash slurry samples (that has been mixed with water) allowing for a lower leachability of elements in the aqueous state; and
- The fly ash samples showed the highest concentration of metal leachate due to no water being mixed with the sample, allowing for a higher available total element concentration.

Synthetic Precipitation Leachate Procedures (SPLP) was performed on each sample type (results listed and compared against drinking water standards in Table 4-5) to evaluate a worst case scenario under slightly acidic conditions (pH 4.8). This provided input into the environmental impact assessments and contaminant transport modelling.

The following conclusions based on the results compared against SANS drinking water standards can be reached:

- The ash slurry sample produced the cleanest leachate with only an alkaline pH again being above recommended values;
- The ash dump and fly ash samples had leachable concentrations of B, Ba, Cr, Mo and TDS, above the recommended guideline values; and
- The cleaner results in both test types on the ash slurry indicate that the potential impact from the new ash dump will be much less than previous dumps.

**Although drinking water standards were used for comparison. These values are not a true reflection of what will reach the receptors and the drinking water standards were only used as a reference value. The waste classification discussed below is the relevant classification to guide the liner requirements.**

### **Waste Classification**

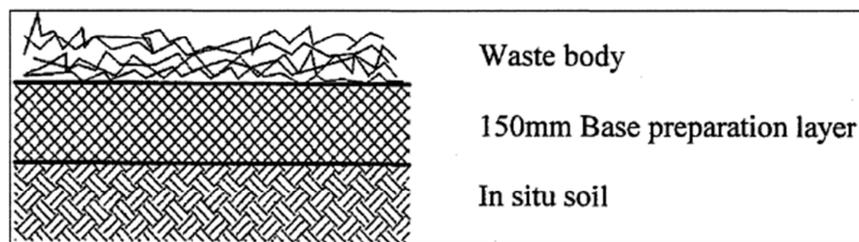
Based on the leachate tests results for waste classification of the ash the following classification of the material according to the NEM: WA guidelines can be made:

- The material has a TC classification of  $TCT_0 < TC \leq TCT_1$ ;
- The material has a LC classification of  $LC \leq LCT_0$ ; and
- The waste can be classified as a Type 3 waste with the waste disposal facility to be designed in accordance to the guidelines for a Class C landfill site shown in Figure 5-1.

**However, following the above conclusions from the interpretation of the results based on the NEM: WA guidelines it should be noted that only the TC values renders this material a Type 3 waste that requires a Class C liner. The leachate (which is the pollution that will be released by the source) is well within the LCT<sub>0</sub> guideline ranges.**

**If a risk based approach is implemented and only the LC values are used this material will be classed as a Type 4 waste which requires a Class D liner, or similar, as shown**

(d) Class D Landfill:



**below.**

### **Liner requirements**

Based on the above study taking into accounts both geochemical and hydrogeological conclusions from the groundwater study and the current groundwater resource state, DWE concluded the following on the need for the ash dumps to be lined based on a risk based approach followed:

- From the geochemical assessment and geohydrological models it has been shown that the potential contamination and environmental impacts from seepage from the ash dumps is a very low risk and not likely based on a conservative approach and simulations. All material was characterised and modelling considered conservative simulations; and
- DWE thus finds that the need for a Class C liner, as stipulated by the waste classification is not necessary as the potential impact for contamination from the dumps is very low and the probability or likelihood of a high volume of contaminants being released is also negligible. Thus, the recommendation based on a risk based approach is for the motivation for a Class D liner or similar design instead.

### Recommendations

- Based on the outcome of the groundwater and geochemical investigations, In order to assess the groundwater level drop and potential impact on groundwater users due to ash dam construction and to assess groundwater deterioration (if any) due to the operation of the ash dam a monitoring programme is required.
- It is recommended that the groundwater monitoring be supplemented with the proposed new boreholes listed in the table below. The exact location of the new boreholes can be altered following a geophysical assessment (Plan 5).

BOREHOLE ID	COORDINATES	
	Latitude	Longitude
BH1A	-26.288147°	29.206993°
BH1B	-26.274230°	29.222923°
BH1C	-26.263444°	29.219698°
BH1D	-26.251490°	29.211249°
BH1E	-26.261808°	29.196200°
BH1F	-26.270432°	29.175587°
BH1G	-26.279813°	29.188151°

- Quarterly monitoring of groundwater quality and levels as per the monitoring program;
- Based on all data considered and a risk based approach implementing the source term-pathway-methodology, it is recommended that a Class D or similar is appropriate

---

for the ash dump as long as good management processes are in place with monitoring data acquired regularly; and

- Integrated water management plan needs to be designed to include storm water management.

## TABLE OF CONTENTS

1	Introduction .....	1
1.1	Project Description.....	1
1.2	Study Objectives.....	1
1.3	Deliverables .....	1
1.4	Report Structure .....	2
2	Methodology .....	3
2.1	Desktop Study .....	3
2.2	Geochemistry.....	3
2.2.1	<i>Sample Distribution and Locations</i> .....	3
2.2.2	<i>Sampling Methodology and Preservation</i> .....	4
2.2.2.1	Fly Ash.....	4
2.2.2.2	Ash Slurry .....	4
2.2.2.3	Ash Dump Material .....	4
2.2.2.4	Sample Preservation .....	4
2.3	Reporting .....	4
3	Project Area Description .....	5
3.1	Topography and Drainage.....	5
3.2	Climate, Rainfall and Groundwater recharge.....	7
3.3	Geology.....	7
4	Geochemistry.....	8
4.1	XRF Results.....	9
4.2	XRD Results .....	11
4.3	ABA and NAG Results.....	12
4.4	Distilled Water Leachate Tests.....	12
4.5	SPLP Tests .....	13
5	Waste Classification .....	17
5.1	Legislative Guidelines.....	17
5.2	Data Evaluation and Comparisons.....	17

---

5.2.1	<i>Total Concentration Threshold</i> .....	17
5.2.2	<i>Leachable Concentration Threshold</i> .....	18
5.3	Classification.....	19
6	Conclusions .....	21
6.1	Geochemistry.....	21
6.2	Waste Classification .....	22
6.3	Liner requirements:.....	22
7	Recommendations .....	23
8	References.....	24

## LIST OF FIGURES

Figure 3-1: Topographical cross-section from north to south (Google Earth).....	6
Figure 3-2: Topographical cross-section from east to west (Google Earth).....	6
Figure 5-1: Type C landfill design.....	19
Figure 5-2: Type D liner design .....	20

## LIST OF TABLES

Table 2-1: Geochemical sample locations .....	4
Table 4-1: Sample ID's and laboratory tests.....	8
Table 4-2: XRF results summary.....	10
Table 4-3: Trace elements compared to crustal averages .....	10
Table 4-4: XRD results summary .....	12
Table 4-5: Distilled water and SPLP leachate results .....	15
Table 5-1: Total Concentration Threshold (TCT) .....	18
Table 5-2: Leachable Concentration Threshold (LCT) .....	18
Table 12-1: Recommended monitoring boreholes.....	23

## LIST OF APPENDICES

Appendix A: Plans

Appendix B: Laboratory Certificates

## 1 Introduction

### 1.1 Project Description

Digby Wells Environmental (Digby Wells) was tasked to perform a geochemical and waste classification assessment for the proposed Kriel power station dump extension project. Kriel Power Station is located approximately 6 km northeast of Matla Coal Mine in the Mpumalanga Province (Appendix A, Plan 1). The existing ash dam at the Kriel Power Station is reaching full capacity and Eskom therefore requires the construction of a new ash dam in order to continue operations. If required, and during ongoing construction of the new ash dam, Eskom plans to transfer ash to the neighbouring Matla Power Station and/or increase the height of the existing facility at Kriel Power Station.

The proposed site for the new ash dam is situated at an old mined-out area, opposite the old ash dam that is in operation; partially filled with ash and spoils material (Appendix A, Plan 1). Although the site selection process recommended this as the preferred site for ash disposal, detailed geotechnical studies will be conducted to quantify the extent of differential settlements. The findings will then be used to finalise the designs of the proposed ash dam extension.

In order to comply with pollution prevention measures, as per the Department of Water and Sanitation's (DWS) Best Practice Guidelines and Eskom's policy of zero harm to the environment, Eskom committed to obtain applicable water use authorisations for the following activities:

- The proposed ash facility;
- Ash transfer link;
- "Step-in and go higher" of the existing facilities; and
- Waste Classification of the ash material.

### 1.2 Study Objectives

The objectives of the geochemical study are as follow:

- Geochemically assess the existing ash dam material, as well as fresh ash material to assist with waste classification of the material;
- Waste classification and liner requirements.

### 1.3 Deliverables

The following deliverables form part of this study:

- Geochemistry assessment;
- Waste classification; and
- Technical report with recommendations.

## 1.4 Report Structure

The remainder of the report is structured as follows:

- Section 2: Methodology
- Section 3: Project Area Description
- Section 4: Geochemistry
- Section 5: Waste Classification
- Section 6: Conclusions
- Section 7: Recommendations

## 2 Methodology

### 2.1 Desktop Study

During this task, available documentation and information related to the project and surrounding areas was sourced from the client and the public domain. Most of the data used in this report is a combination of existing data from previous geohydrological studies (Aurecon, 2011) and data collected during the 2014 hydrocensus and geochemical sampling associated with this study. All data feeds into the impact assessment and groundwater reserve determination.

### 2.2 Geochemistry

Ten (10) samples of ash and spoil material were submitted for geochemical characterisation. The following characterisation tests were conducted:

- The Synthetic Precipitation Leachate Procedure (SPLP) and Distilled water leachate tests (DWLT) are done to simulate the heavy metal and anion leachate potential of the material and water left in-situ under normal conditions with only rain water allowing leaching to occur. These tests will simulate and evaluate the potential of any heavy metal or ion contamination from the ash and spoil material.
- The Acid Base Accounting (ABA) procedure measures the acid- and alkaline-producing potential of the undisturbed material in order to determine if, after disturbance, the ash material will produce acid and subsequently leach metals leading to contamination risks. This procedure includes Net Acid Generation (NAG) tests that evaluate the acid generation and neutralising potential of the material.
- The X-Ray Diffraction (XRD) tests allows for the measurement of the crystal structures within a sample to determine the mineralogical composition of the material. The XRD test is an X-ray method used to determine the elemental composition of a material.

#### 2.2.1 Sample Distribution and Locations

During the site visit on 3 July 2014, ash dump sites 2 and 3 were visited, as well as the mixing plant where fly ash is received and then slurried for deposition onto the ash dumps.

The following sample distribution and locations were used:

- Two (2) dry fly ash samples from the conveyor line before being mixed with water, to represent the geochemistry of the ash before water can allow reactions to take place;
- Four (4) ash slurry samples from the ash stream after the fly ash have been mixed with water to produce the slurry, to represent the fresh material as it will be deposited onto the new facility; and

- Four (4) ash samples from 4 locations on the existing ash dump, to allow for an evaluation of the ash chemistry after leaching and reactions have taken place. The exact positions of these locations were chosen by the samplers based on the accessibility to the points listed in Table 2-1.

**Table 2-1: Geochemical sample locations**

Site ID	Latitude	Longitude
EADS1	-26.265471°	29.202271°
EADS2	-26.268865°	29.202039°
EADS3	-26.266287°	29.196309°
EADS4	-26.270421°	29.192601°

## 2.2.2 Sampling Methodology and Preservation

### 2.2.2.1 Fly Ash

The dry fly ash samples (1 kg in weight) were taken directly from the conveyor line and collected in plastic sampling bags (provided by Digby Wells). The bags were sealed with cable ties and labelled FAS1 and FAS2 with the date of sampling.

### 2.2.2.2 Ash Slurry

The ash slurry samples (2 litres per sample) were collected in glass bottles (provided by Digby Wells). The bottles were sealed and labelled ASS1, ASS2, ASS3 and ASS4 with the date of sampling.

### 2.2.2.3 Ash Dump Material

Samples were taken from the existing ash dump (Table 1) with a soil sampling auger (provided by Digby Wells) up to a depth of approximately 1 m below surface. The samples were collected in plastic sampling bags (provided by Digby Wells). The bags were sealed with cable ties and labelled EADS1, EADS2, EADS3 and EADS4 with the date of sampling.

### 2.2.2.4 Sample Preservation

All samples were sealed and labelled in the supplied containers/bags and stored in a cool dry place out of direct sunlight.

## 2.3 Reporting

A technical report summarising the laboratory results with a completed waste classification and recommendations on the liner requirements.

## 3 Project Area Description

### 3.1 Topography and Drainage

The Kriel Power Station has been constructed in an undulating area, on the crest of a southwest-northeast trending ridge. Springs in the vicinity of Kriel Power Station feed the seasonal Onverwacht, Pampoen and Vaal Pan Spruits (which drain to the east, north and west respectively). Ultimately, all surface water from this area drains into the Olifants River via the Riet (water draining north and west of the ridge) and Steenkool (water draining east) spruits (Aurecon 2011).

The topography of the area is variable due to the nature of mining activities and the subsequent rehabilitation that has taken place. The entire area to the east and south of the complex has been disturbed, either by mining and rehabilitation activities, or by the construction of existing dams. Where the pit has been rehabilitated, the topography is gently undulating, however, there are areas where the dragline tips still form steep cones of spoil. The western final cut void has been filled with ash from the power station and rehabilitated. The eastern final cut void is still open and is partially filled with water. The ground generally slopes towards the southwest.

Two cross sections across the proposed site and study area, one from north to south (Figure 3-1) and the other from east to west (Figure 3-2) show the topography of the area with ash dumps mostly located on the high points.

The proposed site for the new ash dump extension lies within the watersheds of the B11D quaternary catchment, forming part of the Olifants Water Management Area (WMA). The main drainage or stream of the area is the Dwars-in-die-weg spruit which drains into the Olifants River to the north (Appendix A, Plan 2). The topographical changes due to mining and ash dump activities have however developed open pit areas as discussed previously to the east of the proposed extension site. These pits are flooded and act as a drain to which most of the groundwater and surface water is currently flowing.



Figure 3-1: Topographical cross-section from north to south (Google Earth)



Figure 3-2: Topographical cross-section from east to west (Google Earth)

## 3.2 Climate, Rainfall and Groundwater recharge

The climate is typically Highveld conditions, with warm summers (12 to 29 degrees Celsius (°C)) and cold winters (-3 to 20 °C). Frost is usually experienced between May and August (Aurecon, 2011).

According to the *FAO Clim 2.0* database the project area receives an average of 693 mm rain per annum (mm/a). The mean annual evapotranspiration for the area is 1 418 mm/a (Aurecon, 2011). This correlates well with the GRDM database giving MAP as 672 mm/a.

The estimated groundwater recharge of the area is 39.06 mm/a or 5.6% of the Mean Annual Precipitation (MAP). This is based on the available GRDM data.

## 3.3 Geology

According to the published 1:250 000 geological map (2628 East Rand), the area under investigation comprises the Ecca Group, and Dwyka and Vryheid Formations (Appendix A, Plan 3). The sediments of the Vryheid Formation overlie an uneven Dwyka floor, which is controlled by the topography of the pre-Karoo platform upon which the Karoo sediments were deposited. The Vryheid Formation, which is present throughout the Highveld Coal Field, attains 140 meters at the thickest point and contains a number of coal seams, of which four (No. 1, 2, 4 and 5 Seams) are considered to have economic potential (Aurecon, 2011).

The deposition of the Vryheid Formation sediments is largely controlled by the irregular pre-Karoo platform on which they were deposited. The pre-Karoo rocks, consisting mainly of felsites of the Bushveld Igneous Complex, have been glacially sculptured to give rise to uneven basement topography. The thin veneer sediments of the Dwyka Formation, which overlies the pre-Karoo, are generally not thick enough to ameliorate the irregularities in the placated surface, which therefore affected the deposition of the younger Vryheid Formation sediments.

The Ecca sediments consist predominantly of sandstone, siltstone, shale and coal. Combinations of these rock types are found in the form of inter-bedded siltstone, mudstone and coarse grained sandstone. Coarse-grained sandstone is a characteristic of the sediments in the Highveld Area. The overburden thickness and preservation of the coal seams is dependent on the surface geomorphology and the subsurface pre-Karoo basement floor (Aurecon, 2011).

Dolerite intrusions in the form of dykes and sills are present within the Ecca Group. The sills usually precede the dykes, with the latter being emplaced during a later period of tensional forces within the earth's crust. Tectonically, the Karoo sediments are practically undisturbed. Faults are rare. However, fractures are common in competent rocks such as sandstone and coal (Aurecon, 2011).

## 4 Geochemistry

The sole purpose of the geochemistry and waste classification tasks is to supplement and advise the geohydrological study and models. Throughout the study the recommended source term-pathway-receptor methodology was applied to allow a risk based approach. The geochemistry work characterises the sources and feeds into the decision on a proposed liner system.

The samples listed in Table 4-1 were collected as described in section 2.2.2 and submitted for the tests indicated.

**Table 4-1: Sample ID's and laboratory tests**

Sample ID	Material type	Tests done
ASS1	Ash - slurry	XRD, XRF, ABA, NAG and Distilled water leachate test
ASS2	Ash - slurry	XRD, XRF, ABA, NAG and Distilled water leachate test
ASS3	Ash - slurry	XRD, XRF, ABA, NAG and Distilled water leachate test
ASS4	Ash - slurry	XRD, XRF, ABA, NAG and SPLP test
AEDS1	Ash - Dry ash slurry sample from ash dump	XRD, XRF, ABA, NAG and Distilled water leachate test
AEDS2	Ash - Dry ash slurry sample from ash dump	XRD, XRF, ABA, NAG and Distilled water leachate test
AEDS3	Ash - Dry ash slurry sample from ash dump	XRD, XRF, ABA, NAG and Distilled water leachate test
AEDS4	Ash - Dry ash slurry sample from ash dump	XRD, XRF, ABA, NAG and SPLP test
FAS1	Fly ash	XRD, XRF, ABA, NAG and Distilled water leachate test
FAS2	Fly ash	XRD, XRF, ABA, NAG and SPLP test

The current National Environmental Management: Waste Act, 2008 (Act No. 59 of 2008) (NEM:WA) guidelines proposes distilled water (DW)/ reagent water leachate tests according to the Australian Standard Leachate Procedures (ASLP) for waste classification of material to be mono-disposed. As the ash dumps will only receive ash the distilled water tests were performed for the waste classification purposes. To assess a worst case scenario as per standard practice in environmental management projects the SPLP tests were also performed on each sample to allow an evaluation of the bio-available elements that can potentially leach into solution under slightly acidic or acid rain conditions.

Sections 4.1 to 4.5 describe and evaluates the ash dump and fresh ash material, to feed into the environmental impact assessment. The DW test results will also be used in Section 5 for the waste classification of the ash material. Only organic parameters were analysed for in

the leachate procedures on ASS4. This was done to evaluate whether any organics do exist and to save costs on duplicating tests.

#### 4.1 XRF Results

The XRF results summarised in Table 4-2 and Table 4-3 indicate the oxide and trace element distributions for the various samples.

The standard deviation across all samples, for the various oxide distributions is never more than 2.2%. This indicates that possible dissolution and removal of some elements from the reactions with the slurry water and natural leaching of elements on the existing dumps are not a major factor and doesn't affect the mineralogical nature of the ash material. The high SiO<sub>2</sub> content (which is mostly in the form of amorphous material formed due to the high temperatures during burning) lowers the solubility of the material with the low hydraulic conductivity of ash material also aiding in not allowing any elements that does dissolve to leave the system.

The major oxides present in the ash material are SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, Fe<sub>2</sub>O<sub>3</sub>, CaO and MgO. The sulphur content is low with a high lime content (CaO) indicating a low potential for acid generation with a high buffering capacity. On ignition of the test there was a low loss of material as the ash already went through a high temperature procedure with a low moisture content.

The trace element distribution was compared to average crustal values and in most cases is higher than normal. This is however no indication of any potential impacts or leachability. All heavy metals expected in the amorphous ash in small quantities are present with As, B, Ba, Al and Mn mostly prone to dissolve and be removed from the solid system.

**Table 4-2: XRF results summary**

Major Elements	Major Element Concentration (wt %)[s]											
	ASS 3	ASS 2	ASS 1	AEDS 1	AEDS 2	AEDS 3	AEDS 4	FAS 1	FAS 2	Min	Max	St Dev
SiO <sub>2</sub>	49.2 8	48.9 9	51.8 1	47.95	50.34	47.48	48.16	51.3 8	50.5 3	47.4 8	51.8 1	1.5
TiO <sub>2</sub>	1.51	1.5	1.52	1.68	1.6	1.61	1.61	1.73	1.7	1.5	1.73	0.1
Al <sub>2</sub> O <sub>3</sub>	27.9 7	28.3 9	28.5 8	30.34	29.99	30.54	29.3	30.8 2	30.6 6	27.9 7	30.8 2	1.0
Fe <sub>2</sub> O <sub>3</sub>	4.06	3.66	3.92	2.49	2.34	2.43	2.67	2.85	2.65	2.34	4.06	0.6
MnO	0.04	0.04	0.05	0.03	0.03	0.03	0.04	0.03	0.03	0.03	0.05	0.0
MgO	1.27	1.24	1.34	1.4	1.3	1.44	1.35	0.94	0.89	0.89	1.44	0.2
CaO	9.47	9.06	9.57	6.82	6.16	6.99	7.69	7.09	6.82	6.16	9.57	1.2
Na <sub>2</sub> O	0.07	0.05	0.03	0.21	0.18	0.34	0.19	0.12	0.15	0.03	0.34	0.1
K <sub>2</sub> O	0.72	0.73	0.72	0.86	0.87	0.81	0.93	0.68	0.66	0.66	0.93	0.1
P <sub>2</sub> O <sub>5</sub>	0.4	0.39	0.43	0.72	0.59	0.69	0.64	0.56	0.54	0.39	0.72	0.1
Cr <sub>2</sub> O <sub>3</sub>	0.02	0.02	0.02	0.02	0.02	0.04	0.02	0.02	0.02	0.02	0.04	0.0
SO <sub>3</sub>	0.85	0.77	0.6	0.6	0.82	0.83	0.99	0.83	0.83	0.6	0.99	0.1
LOI	2.28	2.52	2.04	7.26	6.11	5.11	6.32	1.7	1.17	1.17	7.26	2.2
H <sub>2</sub> O	0.49	0.53	0.31	1.07	2.07	0.76	1.64	0.1	0.16	0.1	2.07	0.6

**Table 4-3: Trace elements compared to crustal averages**

Trace Elements	Upper continental crust	Trace Element Concentration (ppm) [s]									
		ASS 3	ASS 2	ASS 1	AEDS 1	AEDS 2	AEDS 3	AEDS 4	FAS 1	FAS 2	
As	1.5	1.55	4.33	2.47	15.2	16.3	16.4	15.9	11.3	11.7	
Ba	550	814	798	745	954	932	966	1021	710	729	
Bi	1.27	1.3	1.43	0.9	1.56	1.68	1.84	1.36	1.23	1.4	
Cd	98	4.42	5.03	4.78	4.94	3.55	6.85	5.87	4.98	4.62	
Ce	64	187	127	73.9	108	129	101	101	131	117	
Co	17	<0.56	<0.56	<0.56	<0.56	<0.56	<0.56	<0.56	<0.5	<0.5	
Cs	4.8	2.18	3.8	3.85	4.69	1.85	4.21	7.78	3.2	3.55	
Cu	25	44.8	44	38.2	59.4	58.9	62	57.7	52.6	54	
Ga	17	24.5	24	21.4	45.6	39.8	40.4	40.1	35.3	36	
Ge	1.6	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.5	<0.5	
Hf	5.8	7.37	11.1	3.37	1.92	1.71	6.39	2.95	2.36	6.46	
Hg	9	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<1.0	<1.0	
La	30	23.1	61.1	42.9	34	44.8	39.9	37.6	62	33.4	
Lu	0.32	2.58	2.47	2.37	2.17	2.15	2.25	2.22	2.29	2.27	
Mo	1.5	2.35	2.31	2.35	2.28	2.23	2.3	2.27	2.26	2.25	
Nb	12.5	32.9	36.4	31.5	41.3	39.2	40.2	40.8	37.8	37.3	
Nd	26	<2.39	<2.39	<2.39	35.6	44	58	46.4	<2.3	<2.3	
Ni	50	39.1	34.8	34.2	51	45.5	53.2	39.4	54.2	46.2	
Pb	16	<2.03	<2.03	<2.03	100	101	111	91	68.6	71.4	
Rb	112	32.7	35.7	29.9	55.5	53	50.8	57.7	38.4	39.1	
Sb	0.2	4.63	<1.48	<1.48	4.4	4.64	2.66	<1.48	<1.4 8	2.79	
Sc	13	35	43.2	38.3	33.5	31.4	33.3	35.8	31.2	34	
Se	50	3.02	2.24	2.87	8.99	7.36	8.58	6.86	5.51	6.07	
Sm	4.5	14.5	14.9	14.1	3.37	7.26	4.38	6.11	8.18	10.5	

Trace Elements	Upper continental crust	Trace Element Concentration (ppm) [s]								
		ASS 3	ASS 2	ASS 1	AEDS 1	AEDS 2	AEDS 3	AEDS 4	FAS 1	FAS 2
Sn	5.5	18.5	14.5	12.5	18.5	18.4	17.5	19.5	15.5	14.5
Sr	350	1908	1893	1723	2569	1928	2388	2340	1595	1607
Ta	1.1	1.21	1.54	1.82	1.43	1.35	1.61	1.62	2.19	1.76
Th	10.7	25.6	24.7	25.6	33.3	29	30.3	32.3	32.3	30.9
Tl	0.75	0.71	0.65	0.37	1.06	0.78	0.95	1.25	0.87	0.84
U	2.8	14.9	13.6	13.2	23.1	15.3	20.3	18.2	13.8	13.9
V	110	<7.60	<7.60	<7.60	<7.60	<7.60	<7.60	<7.60	<7.6	<7.6
W	2	1.33	1.32	1.26	1.18	1.16	1.16	1.3	1.13	1.22
Y	22	67.3	68.2	61.5	80.6	74.4	76.4	79.5	70.3	71.2
Yb	2.2	10.1	10.1	7.34	5.81	4.84	6.8	7.28	3.77	8.88
Zn	71	32	30.8	30.9	55.3	52.3	50.8	47.5	46.6	43.5
Zr	190	479	483	444	535	478	518	521	473	479

## 4.2 XRD Results

The XRD results summarised in Table 4-4 shows that minerals formed through the combination of the trace elements and oxides discussed in section 4.1. The high silica content was distributed mainly between the amorphous (glass) and quartz minerals. The high iron content observed in the XRF results was distributed between hematite, magnetite and pyrite, with mullite and lime completing the mineral content distribution.

The process in which the ash is produced at high temperatures lead to high aluminium silicate content with iron and calcium based minerals left. The pyrite content can potentially lead to acid formation. However, a high calcite and lime content with high buffering capacity and the low reactivity of silica will counter any acid production with neutralising reactions.

The following are the ideal chemical formulas for each mineral:

<b>Quartz:</b>	SiO <sub>2</sub>
<b>Plagioclase:</b>	(Na, Ca)Al <sub>2</sub> Si <sub>3</sub> O <sub>8</sub>
<b>Lime:</b>	CaO
<b>Magnetite:</b>	Fe <sub>3</sub> O <sub>4</sub>
<b>Pyrite:</b>	Fe S <sub>2</sub>
<b>Calcite:</b>	CaCO <sub>3</sub>
<b>Mullite:</b>	Al <sub>4,5</sub> Si <sub>1,5</sub> O <sub>9,75</sub>
<b>Hematite:</b>	Fe <sub>2</sub> O <sub>3</sub>

**Table 4-4: XRD results summary**

Mineral	Mineral weight %								
	ASS3	ASS2	ASS1	AEDS1	AEDS2	AEDS3	AEDS4	FAS1	FAS2
Amorphous	39.33	34.54	39.75	36.51	38.06	35.57	37.9	37.14	39.86
Calcite	0.99	1.5	2.53	5.94	2.45	4.3	3.95	0.63	0
Hematite	2.02	2.05	1.6	0.14	0.42	0.38	0.45	0.92	0.92
Magnetite	3.77	3.79	3.1	2.87	2.55	2.59	2.62	3.55	3.48
Mullite	19.97	22.47	19.05	35.48	34.49	36.13	32.64	34.05	35.4
Plagioclase	18.08	18.2	19.29	2.7	1.45	3.79	3.17	1.78	0
Pyrite	0.25	0.41	0.47	0.32	0.76	0.6	0.57	0.54	0.41
Quartz	15.6	17.03	14.22	16.04	19.83	16.65	18.7	19.22	17.97
Lime	-	-	-	-	-	-	-	2.18	1.96
<b>Total</b>	<b>100</b>	<b>100</b>	<b>100</b>	<b>100</b>	<b>100</b>	<b>100</b>	<b>100</b>	<b>100</b>	<b>100</b>

### 4.3 ABA and NAG Results

The Acid Base Accounting (ABA) and Net Acid Generation (NAG) tests performed on the ash samples allow for an evaluation of any potential for acid generation from the material analysed. The ABA and NAG results given in Appendix B can be summarised as follows:

- All samples have a paste pH of above 11 which is well above the acid producing margin of pH 5. This shows that the material is highly alkaline with a buffering potential. The high pH can however lead to dissolution and higher aqueous activity of metals like Al and B;
- The total sulphur concentrations in all samples are below the recommended 0.3%. Above the 0.3% value material will have an acid generating potential;
- The Neutralising Potential Ratio (AP:NP) is well above 4:1 indicating that the nett neutralising capacity of the material is much higher than any potential for acid production;
- Along with the high NPR, all samples show no NAG potential (all values are lower than 0.01) and thus all the ash samples can be classified as non-acid generating; and
- Although no acid generation is predicted there is still a potential for certain elements to leach at high pH levels.

### 4.4 Distilled Water Leachate Tests

Distilled water tests were performed on two fresh ash slurry samples (ASS3 and ASS2), three ash samples from the existing ash dumps (AEDS1, AEDS2 and AEDS3) and one fly ash sample (FAS1) before being mixed with process water to produce slurry.

The tests on the existing ash dump and fly ash samples were to assess and compare the potential changes in material behaviour under normal, neutral leaching conditions. The following conclusions have been reached from the results presented in Table 4-5:

- The two fresh samples submitted for testing according to NEM:WA guidelines showed the best leachate quality results with all parameters of concern below the SANS drinking water guideline values with the exception of pH;
- Both samples showed leachable pH levels above 10 indicating (as mentioned in the mineralogical and ABA interpretations) a high buffering capacity;
- The fly ash and existing ash dump samples however showed leachable concentrations of B, Ba, Cr, Mo and TDS; above the recommended limits for drinking water;
- The higher leachability in these samples can be due to the fresh ash slurry samples (that has been mixed with water) allowing for a lower leachability of elements in the aqueous state; and
- The fly ash samples showed the highest concentration of metal leach due to no water being mixed with the sample allowing for a higher available total element concentration.

#### 4.5 SPLP Tests

Synthetic Precipitation Leachate Procedures (SPLP) were performed on each sample (results listed and compared against drinking water standards in Table 4-5) to evaluate a worst case scenario under slightly acidic conditions (pH 4.8); to provide input into the environmental impact assessments and contaminant transport modelling.

The following conclusions, for results compared against SANS drinking water standards can be reached:

- The ash slurry sample produced the best quality leachate, with only an alkaline pH being above recommended values;
- The ash dump and fly ash samples had leachable concentrations of B, Ba, Cr, Mo and TDS; above the recommended guidelines; and
- The better quality results in both ash slurry tests indicate that the potential impact from the new ash dump will be much less than previous dumps.

**Although drinking water standards were used for comparison in this section of the report. These values are not a true reflection of what will reach the receptors and the drinking water standards were only used as a reference value. The waste classification discussed below is the relevant classification to guide the liner requirements. The drinking water standards are more stringent than the LCT values.**



**Table 4-5: Distilled water and SPLP leachate results**

Sample ID	SANS 241:2011 Drinking water guidelines	ASS3	ASS2	AEDS1	AEDS2	AEDS3	FAS1	ASS1	AEDS4	FAS2
Test method		Distilled Water	SPLP	SPLP	SPLP					
Units	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
As, Arsenic	0.01	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010
B, Boron	0.5	0.167	0.104	1.27	0.801	0.997	0.848	0.232	0.518	0.868
Ba, Barium	0.7	0.174	0.195	<0.025	0.028	0.033	2.18	0.126	0.048	2.05
Cd, Cadmium	0.003	<0.003	<0.003	<0.003	<0.003	<0.003	<0.003	<0.003	<0.003	<0.003
Co, Cobalt	0.5	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025
Cr <sub>Total</sub> , Chromium Total	0.05	<0.025	0.036	0.142	0.220	0.141	0.238	<0.025	0.240	0.138
Cu, Copper	2	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025
Hg, Mercury	0.006	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001
Mn, Manganese	0.5	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025
Mo, Molybdenum	0.07	<0.025	<0.025	0.052	0.107	0.027	0.107	<0.025	0.026	0.106
Ni, Nickel	0.07	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025
Pb, Lead	0.01	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010
Sb, Antimony	0.02	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010
Se, Selenium	0.01	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010
V, Vanadium	0.2	<0.025	<0.025	0.136	0.075	0.070	<0.025	<0.025	0.037	<0.025
Zn, Zinc	5	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025	<0.025
Total Dissolved Solids*	1200	222	192	152	150	170	1650	178	192	1692
Chloride as Cl	300	<5	<5	<5	<5	<5	<5	<5	<5	<5
Sulphate as SO <sub>4</sub>	500	63	50	61	69	74	143	81	72	98
Nitrate as N	11	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2

Sample ID	SANS 241:2011 Drinking water guidelines	ASS3	ASS2	AEDS1	AEDS2	AEDS3	FAS1	ASS1	AEDS4	FAS2
Test method		Distilled Water	SPLP	SPLP	SPLP					
Units	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
Fluoride as F	<b>1.5</b>	<0.2	<0.2	<0.2	<0.2	<0.2	0.8	<0.2	<0.2	0.9
Total Cyanide as CN	<b>0.07</b>	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05
pH	<b>5 -9.7</b>	11.2	11.4	10.6	10.8	10.9	12.2	10.8	11.0	12.3

## 5 Waste Classification

### 5.1 Legislative Guidelines

The following legislative guidelines were instated during August 2013 and provide the background and guidelines for waste classification in South Africa:

- NEM:WA National Waste Information Regulations, 2012 (DEA 2012);
- NEM:WA National Norms and Standards for the Assessment of Waste for Landfill Disposal (DEA 2013a);
- NEM:WA National Norms and Standards for the Disposal of Waste to Landfill (DEA 2013b); and
- NEM:WA National Waste Classification and Management Regulations (DEA 2013c).

### 5.2 Data Evaluation and Comparisons

The distilled water tests performed on samples ASS1, ASS2, ASS3 and ASS4 (all samples taken from the ash slurry that will be dumped on the new dump site); in accordance with the classification guidelines for mono-disposal sites, were classed against the various thresholds for total concentrations (TC) and leachable concentrations (LC). ASS4's fluid phase was submitted for organic analysis to confirm that no organic material is present. TC analysis was done on all samples, with distilled/reagent water tests done for LC analysis only on ASS3 and ASS2 with ASS submitted for SPLP analysis as discussed in section 4.5.

#### 5.2.1 Total Concentration Threshold

The following classification, also shown in Table 5-1 was made based on the total concentrations threshold (TCT) classes for ASS1, ASS2 and ASS3:

- Barium (Ba), selenium (Se) and fluoride (F) exceed the TCT0 guideline values and fall within the limits of TCT1; and
- All other elements are below the TCT0 guideline values.

**Table 5-1: Total Concentration Threshold (TCT)**

Sample ID	NEM:WA Total Concentration Thresholds			ASS3	ASS2	ASS1
	TCT0	TCT1	TCT2			
<b>Units</b>	<b>mg/kg</b>	<b>mg/kg</b>	<b>mg/kg</b>	<b>mg/kg</b>	<b>mg/kg</b>	<b>mg/kg</b>
As, Arsenic	5.8	500	2000	<4.00	<4.00	<4.00
B, Boron	150	15000	60000	32.4	32	34.4
Ba, Barium	62.5	6250	25000	656	684	708
Cd, Cadmium	7.5	260	1040	3.6	3.6	3.6
Co, Cobalt	50	5000	20000	<10	<10	<10
Cr <sub>Total</sub> , Chromium Total [s]	46000	800000	N/A	60.8	47.2	54.4
Cu, Copper	16	19500	78000	<10	<10	<10
Hg, Mercury	0.93	160	640	<0.4	<0.4	<0.4
Mn, Manganese	1000	25000	100000	305.2	320	335.6
Mo, Molybdenum	40	1000	4000	<10	<10	<10
Ni, Nickel	91	10600	42400	25.6	24.8	27.2
Pb, Lead	20	1900	7600	<8.00	<8.00	<8.00
Sb, Antimony	10	75	300	<4.00	<4.00	4.8
Se, Selenium	10	50	200	10.4	20	8.8
V, Vanadium	150	2680	10720	<10	<10	<10
Zn, Zinc	240	160000	640000	<10	<10	<10
Total Fluoride [s] mg/kg	100	10000	40000	185	253	263
Total Cyanide as CN mg/kg	14	10500	42000	<0.01	<0.01	<0.01

### 5.2.2 Leachable Concentration Threshold

The following classification also shown in Table 5-2 was made based on the leachable concentrations threshold (LCT) classes in ASS3 and ASS2:

- All samples fall within the limits of LCT0.

**Table 5-2: Leachable Concentration Threshold (LCT)**

Parameters	NEM:WA Leachable Concentration Thresholds				Distilled water test samples	
	LCT0	LCT1	LCT2	LCT3	ASS3	ASS2
<b>Units</b>	<b>mg/L</b>	<b>mg/L</b>	<b>mg/L</b>	<b>mg/L</b>	<b>mg/L</b>	<b>mg/L</b>
As, Arsenic	0.01	0.5	1	4	<0.010	<0.010
B, Boron	0.5	25	50	200	0.167	0.104
Ba, Barium	0.7	35	70	280	0.174	0.195
Cd, Cadmium	0.003	0.15	0.3	1.2	<0.003	<0.003
Co, Cobalt	0.5	25	50	200	<0.025	<0.025
Cr <sub>Total</sub> , Chromium Total	0.1	5	10	40	<0.025	0.036
Cr(VI), Chromium (VI)	0.05	2.5	5	20	<0.010	0.029
Cu, Copper	2	100	200	800	<0.025	<0.025

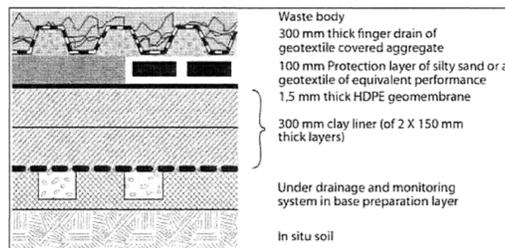
Parameters	NEM:WA Leachable Concentration Thresholds				Distilled water test samples	
	LCT0	LCT1	LCT2	LCT3	ASS3	ASS2
Units	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
Hg, Mercury	0.006	0.3	0.6	2.4	<0.001	<0.001
Mn, Manganese	0.5	25	50	200	<0.025	<0.025
Mo, Molybdenum	0.07	3.5	7	28	<0.025	<0.025
Ni, Nickel	0.07	3.5	7	28	<0.025	<0.025
Pb, Lead	0.01	0.5	1	4	<0.010	<0.010
Sb, Antimony	0.02	1	2	8	<0.010	<0.010
Se, Selenium	0.01	0.5	1	4	<0.010	<0.010
V, Vanadium	0.2	10	20	80	<0.025	<0.025
Zn, Zinc	5	250	500	2000	<0.025	<0.025
Total Dissolved Solids*	1000	12500	25000	100000	222	192
Chloride as Cl	300	15000	30000	120000	<5	<5
Sulphate as SO <sub>4</sub>	250	12500	25000	100000	63	50
Nitrate as N	11	550	1100	4400	<0.2	<0.2
Fluoride as F	1.5	75	150	600	<0.2	<0.2
Total Cyanide as CN	0.07	3.5	7	28	<0.05	<0.05

### 5.3 Classification

Based on the leachate tests the following classification of the material (according to the NEM: WA guidelines) can be made:

- The material has a TC classification of  $TCT0 < TC \leq TCT1$ ;
- The material has a LC classification of  $LC \leq LCT0$ ; and
- The waste can be classified as a Type 3 waste, with the waste disposal facility to be designed in accordance to the guidelines for a Class C landfill site shown in Figure 5-1.

**Figure 5-1: Type C landfill design**

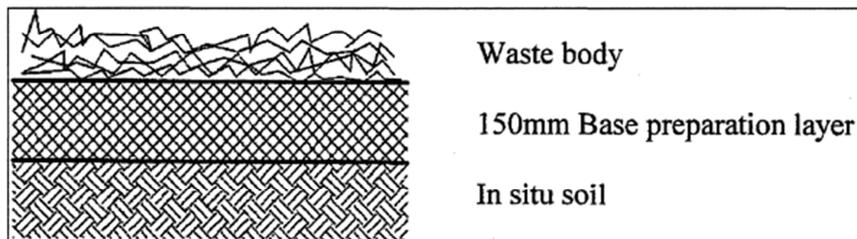


However, following the above conclusions from the interpretation of the results based on the NEM: WA guidelines it should be noted that only the TC values renders this material a Type

3 waste that requires a Class C liner. The leachate (which is the pollution that will be released by the source) is well within the LCT0 guideline ranges.

If a risk based approach is implemented and only the LC values are used this material will be classed as a Type 4 waste which requires a Class D liner, or similar, as shown below in Figure 5-2.

(d) Class D Landfill:



**Figure 5-2: Type D liner design**

## 6 Conclusions

### 6.1 Geochemistry

The ABA and NAG tests performed on the ash samples allowed for an evaluation of any potential for acid generation from the material analysed. The test ABA and NAG results (given in Appendix B) can be summarised as follows:

- All samples have a paste pH of above 11 which is well above the acid producing margin of pH 5. This shows that the material is highly alkaline with a buffering potential. The high pH can however lead to dissolution and higher aqueous activity of metals like Al and B;
- The total sulphur concentrations in all samples are below the recommended 0.3%;
- The Neutralising Potential Ratio (AP:NP) is well above 4:1 indicating that the nett neutralising capacity of the material is much higher than any potential for acid production;
- Along with the high NPR, all samples show no NAG potential (all values are less than 0.01) and thus all the ash samples can be classified as non-acid generating; and
- Although no acid generation is predicted there is still a potential for certain elements to leach at high pH levels.

Distilled water tests were performed on two fresh ash slurry samples (ASS3 and ASS2), three ash samples from the existing ash dumps (AEDS1, AEDS2 and AEDS3) and one fly ash sample (FAS1), before being mixed with process water to produce slurry.

The tests on the existing ash dump samples and fly ash samples were to assess and compare the potential changes in material behaviour under normal neutral leaching conditions. The following conclusions have been reached from the results presented in Table 4-5:

- The two fresh samples submitted for testing according to NEM:WA guidelines showed the best leachate quality results with all parameters of concern below the SANS drinking water guideline values, with the exception of pH;
- Both samples showed leachable pH levels above 10 indicating, as mentioned in the mineralogical and ABA interpretations, a high buffering capacity;
- The fly ash and existing ash dump samples however showed leachable concentrations of B, Ba, Cr, Mo and TDS above the recommended limits for drinking water;
- The higher leachability in these samples can be due to the fresh ash slurry samples (that has been mixed with water) allowing for a lower leachability of elements in the aqueous state; and

- The fly ash samples showed the highest concentration of metal leachate due to no water being mixed with the sample, allowing for a higher available total element concentration.

Synthetic Precipitation Leachate Procedures (SPLP) were performed on each sample type (results listed and compared against drinking water standards in Table 4-5) to evaluate a worst case scenario under slightly acidic conditions (pH 4.8). This provided input into the environmental impact assessments and contaminant transport modelling.

The following conclusions based on the results compared against SANS drinking water standards can be reached:

- The ash slurry sample produced the cleanest leachate with only an alkaline pH again being above recommended values;
- The ash dump and fly ash samples had leachable concentrations of B, Ba, Cr, Mo and TDS, above the recommended guideline values; and
- The cleaner results in both test types on the ash slurry indicate that the potential impact from the new ash dump will be much less than previous dumps.

## 6.2 Waste Classification

Based on the leachate tests results for waste classification of the ash the following classification of the material according to the NEM: WA guidelines can be made:

- The waste can be classified as a Type 3 waste, with the waste disposal facility to be designed in accordance to the guidelines for a Class C landfill site shown in Figure 5-1.
- However, following the above conclusions from the interpretation of the results based on the NEM: WA guidelines it should be noted that only the TC values renders this material a Type 3 waste that requires a Class C liner. The leachate (which is the pollution that will be released by the source) is well within the LCT0 guideline ranges.
- If a risk based approach is implemented and only the LC values are used this material will be classed as a Type 4 waste which requires a Class D liner, or similar as shown in Figure 5-2.

## 6.3 Liner requirements:

Based on the above study taking into account both geochemical and hydrogeological conclusions and the current groundwater resource state DWE concluded the following on the need for the ash dumps to be lined:

- From the geochemical assessment and geohydrological models it has been shown that the potential contamination and environmental impacts from seepage from the ash dumps is a very low risk and not likely based on a conservative approach and

simulations. All material was characterised and modelling considered conservative simulations; and

- DWE thus finds that the need for a Class C liner, as stipulated by the waste classification is not necessary as the potential impact for contamination from the dumps is very low and the probability or likelihood of a high volume of contaminants being released is also negligible. Thus, the recommendation based on a risk based approach is for the motivation for a Class D liner or similar design instead.

## 7 Recommendations

Based on the outcome of the groundwater and geochemical investigations, In order to assess the groundwater level drop and potential impact on groundwater users due to ash dam construction and to assess groundwater deterioration (if any) due to the operation of the ash dam a monitoring programme is required.

- It is recommended that the groundwater monitoring be supplemented with the proposed new boreholes listed in. The exact location of the new boreholes can be altered following a geophysical assessment (plan 5).

**Table 7-1: Recommended monitoring boreholes**

BOREHOLE ID	COORDINATES	
	Latitude	Longitude
BH1A	-26.288147°	29.206993°
BH1B	-26.274230°	29.222923°
BH1C	-26.263444°	29.219698°
BH1D	-26.251490°	29.211249°
BH1E	-26.261808°	29.196200°
BH1F	-26.270432°	29.175587°
BH1G	-26.279813°	29.188151°

- Quarterly monitoring of groundwater quality and levels as per the monitoring program;
- Based on all data considered and a risk based approach implementing the source term-pathway-methodology, it is recommended that a Class D or similar is appropriate

for the ash dump as long as good management processes are in place with monitoring data acquired regularly; and

- Integrated water management plan needs to be designed to include storm water management.

## 8 References

Aurecon, 2011. *Geohydrological Evaluation for the Environmental Impact Assessment*,

DEA, 2013a. *National Norms and Standards for the Assessment of Waste for Landfill Disposal*, Department of Environmental Affairs.

DEA, 2013b. *National Norms and Standards for the Disposal of Waste to Landfill*,

DEA, 2013c. *National Waste Classification and Management Regulations*, Department of Environmental Affairs.

DEA, 2012. *National Waste Information Regulations, 2012*, Department of Environmental Affairs.

Hodgson F.D.I, Krantz R.M, 1995, Investigation into Groundwater Quality Deterioration in the Olifants River Catchment Above the Loskop Dam with Specialised Investigation in the Witbank Dam Sub-Catchment, Bloemfontein.

South African National Standards, 2005. SA Drinking Water Standards - SANS 241:2011.

Geochemistry and Waste Classification **Assessment**

Kriel Power Station Ash Dump Extension

ESK2840



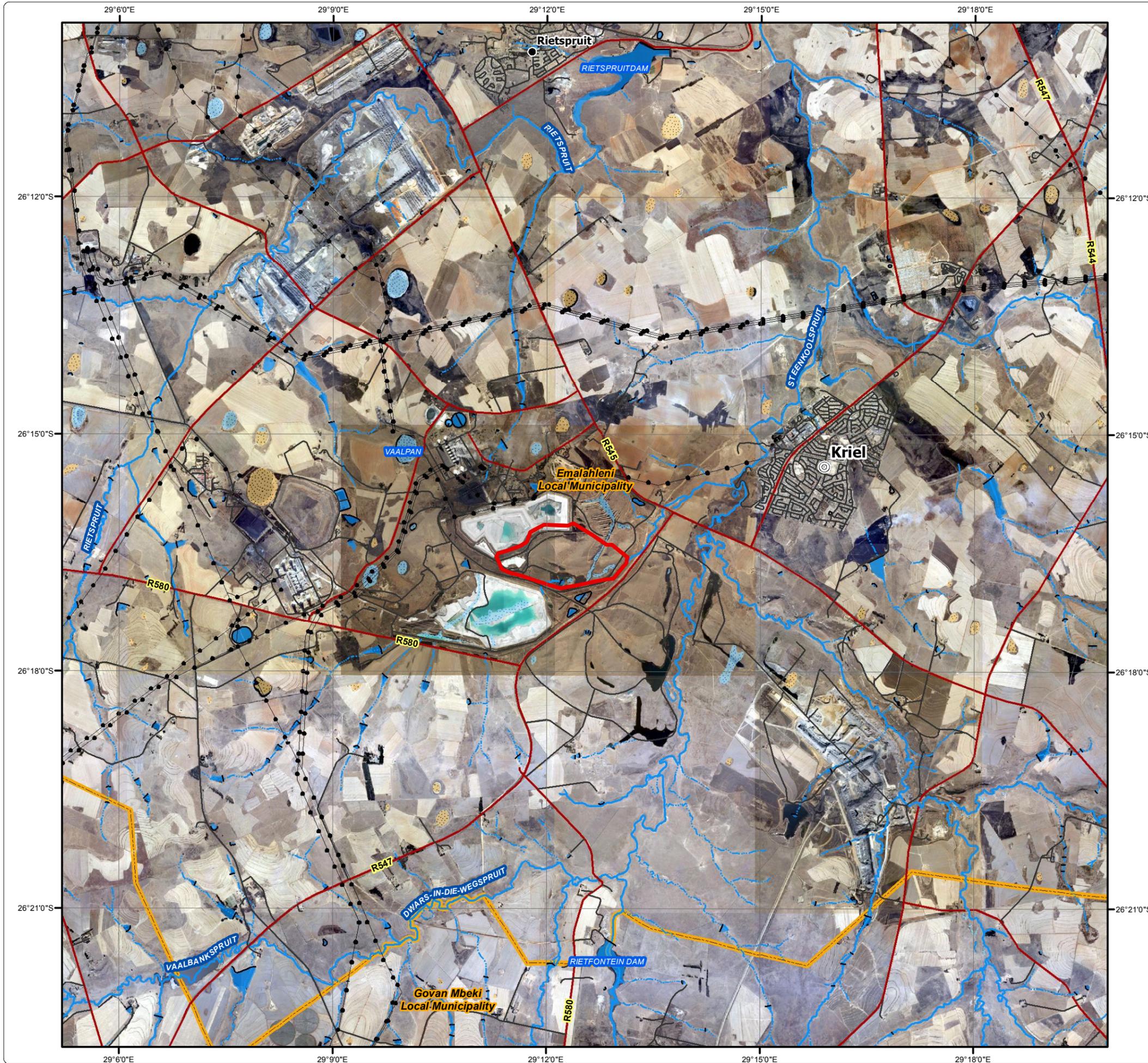
## Appendix A: Plans

# Kriel Power Station IWULA

## Local Setting

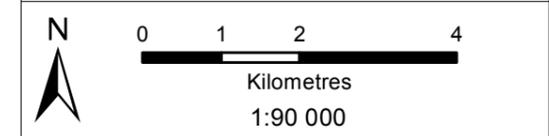
### Legend

- Project Area
- Secondary Town
- Settlement
- Power Line
- Main Road
- Minor Road
- Dam Wall
- Non-Perennial Stream
- Perennial Stream
- Dam / Lake
- Non-Perennial Pan
- Perennial Pan
- Local Municipal Boundary



• Sustainability • Service • Positive Change • Professionalism • Future Focused • Integrity

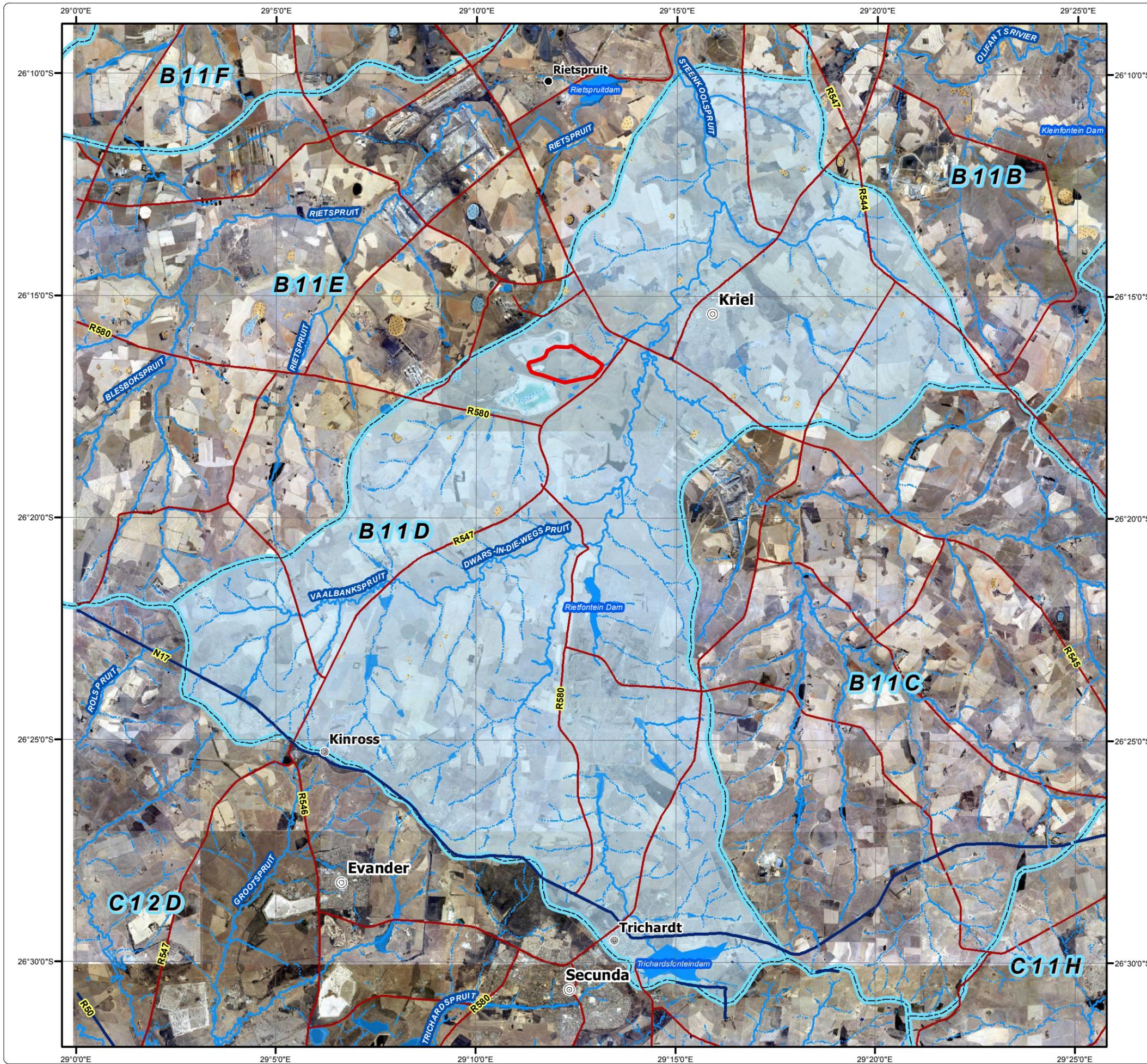
Projection: Transverse Mercator Ref #: mpl.ESK2840.201409.113  
 Datum: Cape Revision Number: 1  
 Central Meridian: 29°E Date: 31/10/2014



# Kriel Power Station IWULA Quaternary Catchment

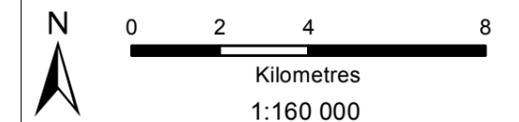
## Legend

-  Project Area
-  Secondary Town
-  Other Town
-  Settlement
-  Arterial/ National Route
-  Main Road
-  Non-Perennial Stream
-  Perennial Stream
-  Dam / Lake
-  Non-Perennial Pan
-  Perennial Pan
-  Affected Quaternary Catchment
-  Quaternary Catchments



• Sustainability • Service • Positive Change • Professionalism • Future Focused • Integrity

Projection: Transverse Mercator      Ref #: mpl.ESK2840.201409.114  
 Datum: Cape      Revision Number: 1  
 Central Meridian: 29°E      Date: 25/09/2014



# Kriel Power Station IWULA

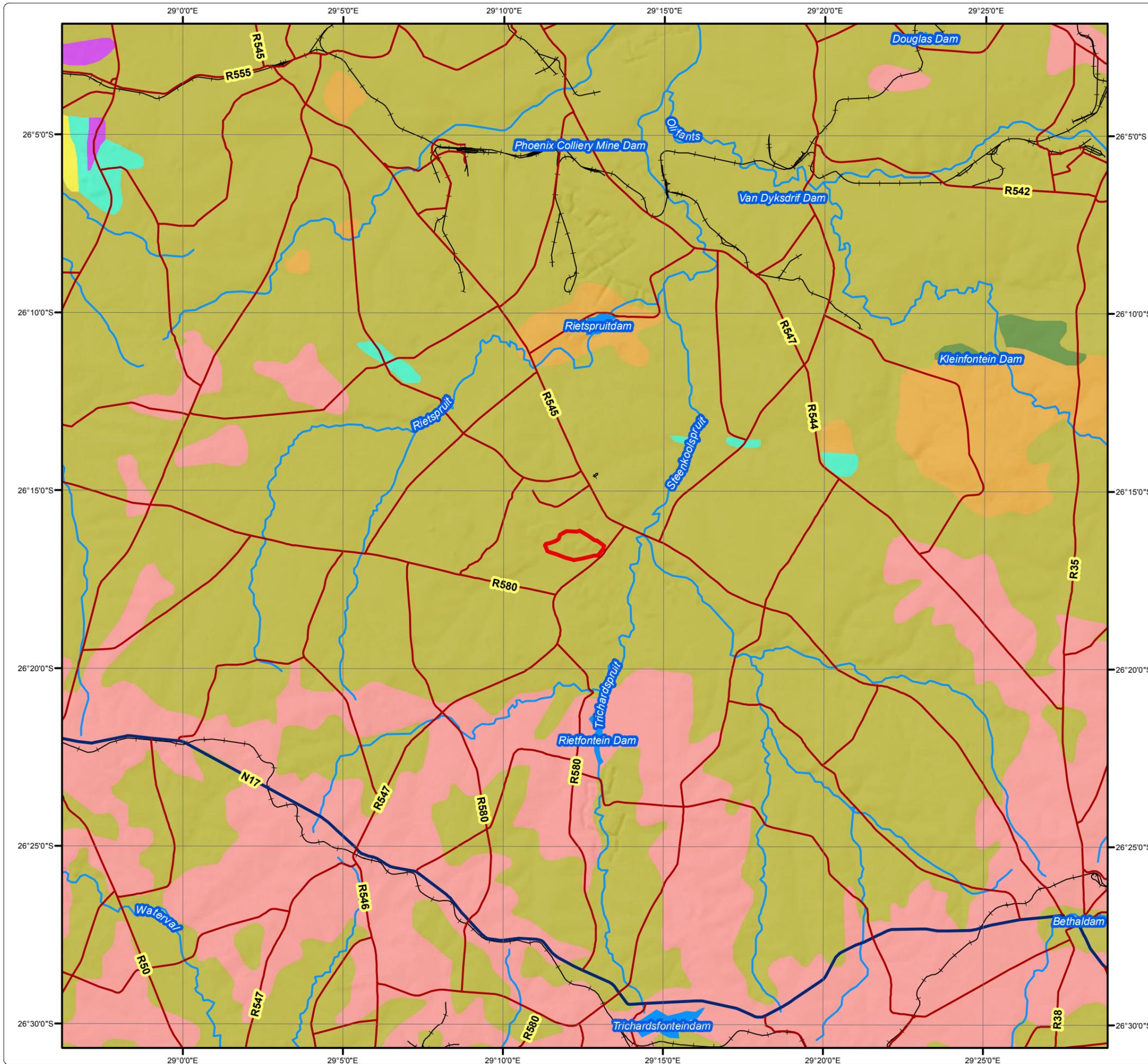
## Regional Geology

### Legend

-  Project Area
-  Main Road
-  Arterial / National Route
-  Railway Line
-  Perennial Stream
-  Dam/ Lake

### Regional Geology

-  Dwarsfontein Cplx
-  Karoo Dolerite Sui
-  Lebowa Granite Sui, Bushveld Cplx
-  Loskop Fm, Transvaal Spgrp
-  Madzaringwe Fm, Karoo Spgrp
-  Rooiberg Grp, Transvaal Spgrp
-  Vaalian Erathem



• Sustainability • Service • Positive Change • Professionalism • Future Focused • Integrity

Projection: Transverse Mercator      Ref #: mpl.ESK2840.201412.049  
 Datum: Cape      Revision Number: 1  
 Central Meridian: 29°E      Date: 31/10/2014

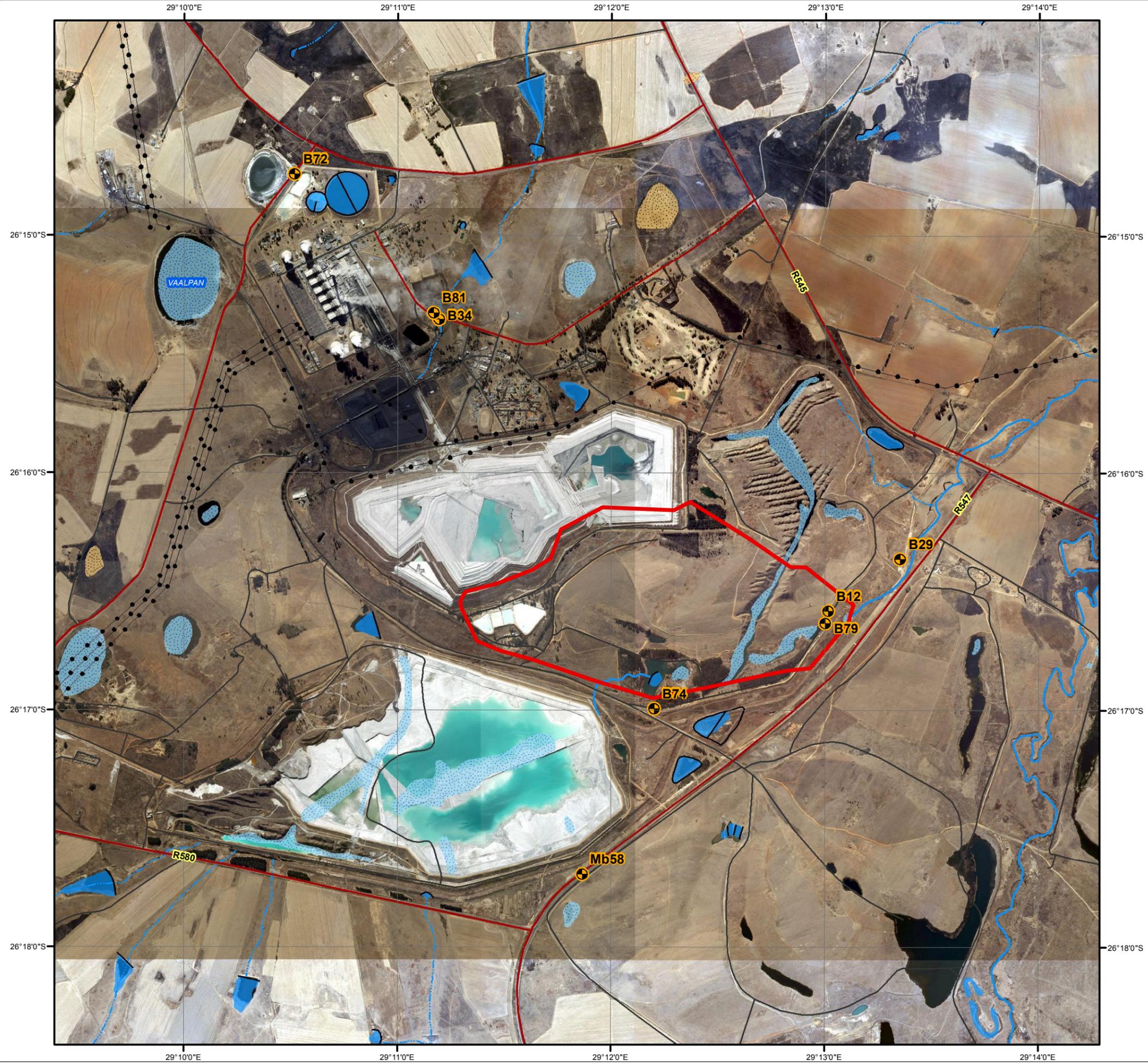


# Kriel Power Station IWULA

## Hydrocensus Boreholes

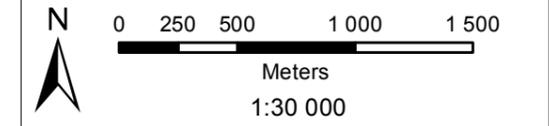
### Legend

-  Project Area
-  Hydrocensus Boreholes
-  Power Line
-  Main Road
-  Minor Road
-  Dam Wall
-  Non-Perennial Stream
-  Perennial Stream
-  Dam / Lake
-  Non-Perennial Pan
-  Perennial Pan



• Sustainability • Service • Positive Change • Professionalism • Future Focused • Integrity

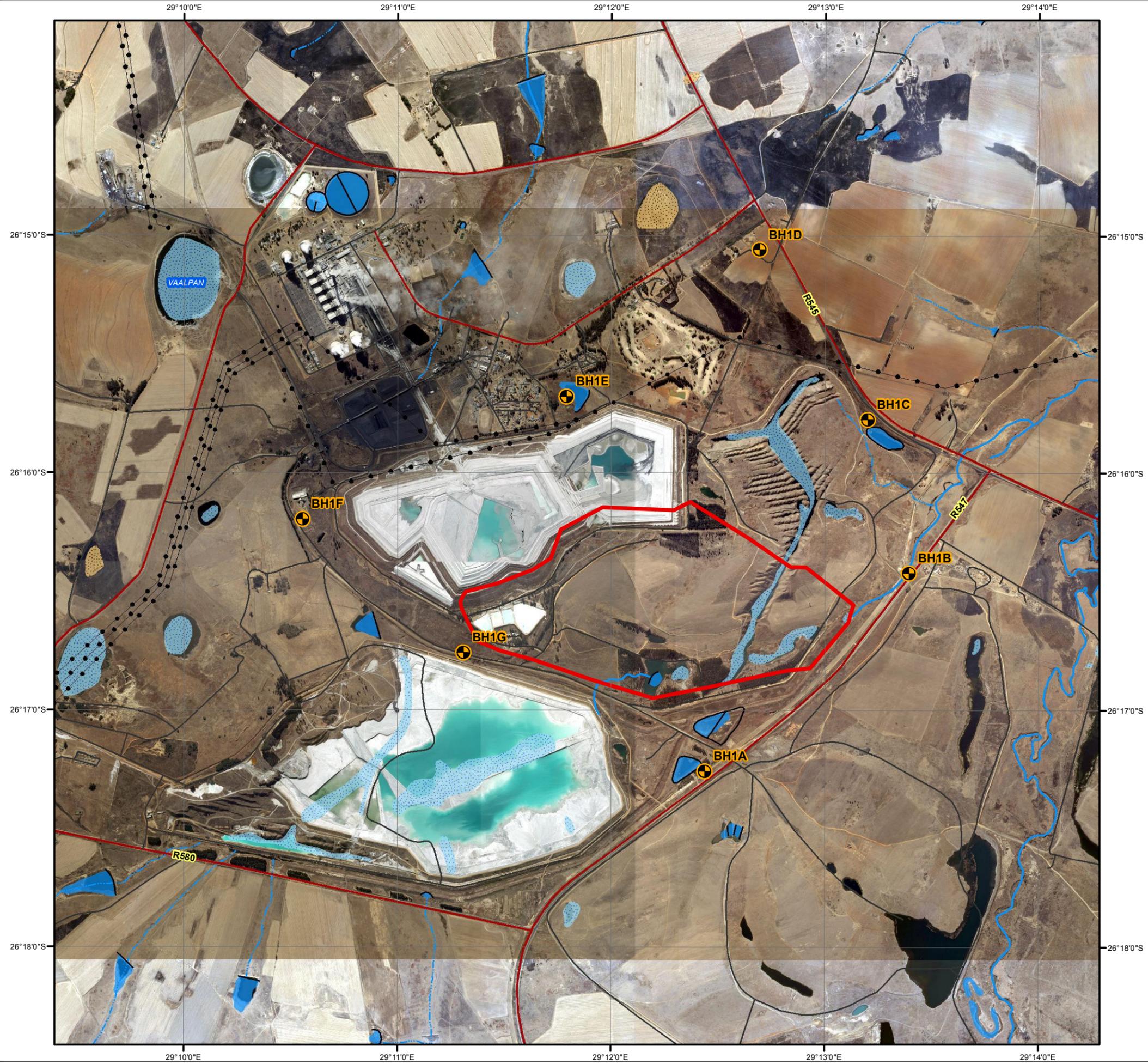
Projection: Transverse Mercator Ref #: mpl.ESK2840.201411.075  
 Datum: Cape Revision Number: 1  
 Central Meridian: 29°E Date: 17/11/2014



# Kriel Power Station IWULA Recommended Monitoring Boreholes

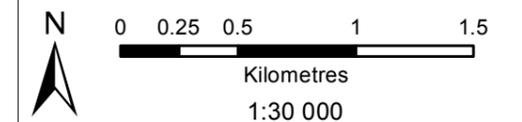
## Legend

- Project Area
- ⊕ Recommended Monitoring Borehole
- Power Line
- Main Road
- Minor Road
- Dam Wall
- Non-Perennial Stream
- Perennial Stream
- Dam / Lake
- Non-Perennial Pan
- Perennial Pan



• Sustainability • Service • Positive Change • Professionalism • Future Focused • Integrity

Projection: Transverse Mercator      Ref #: mpl.ESK2840.201412.105  
 Datum: Cape      Revision Number: 1  
 Central Meridian: 29°E      Date: 11/12/2014



## Appendix B: Laboratory Certificates



## WATERLAB (PTY) LTD

Building D, The Woods,  
Perseus Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

### CERTIFICATE OF ANALYSES NETT ACID GENERATION

Date received: 2014-09-23  
Project number: 1000

Report number: 48142

Date completed: 2014-10-17  
Order number: ESK2840

Client name: Digby Wells Environmental  
Address: Private Bag X 10046, Randburg, 2125  
Telephone: 011 789 9495

Facsimile: 011 789 9498

Contact person: Andre van Coller  
Email: [andre.van.coller@digbywells.com](mailto:andre.van.coller@digbywells.com)  
Cell: 076 076

Nett Acid Generation	Sample Identification: pH 4.5 & 7.0				
	ASS3	ASS2	ASS1	AEDS1	AEDS2
Sample Number	16516	16517	16518	16519	16520
NAG pH: (H <sub>2</sub> O <sub>2</sub> )	9.4	9.6	9.5	9.8	9.9
Titration with NaOH	0.00	0.00	0.00	0.00	0.00
Final pH: (H <sub>2</sub> O <sub>2</sub> )	9.4	9.6	9.5	9.8	9.9
NAG (kg H <sub>2</sub> SO <sub>4</sub> / t)	<0.01	<0.01	<0.01	<0.01	<0.01

Nett Acid Generation	Sample Identification: pH 4.5 & 7.0				
	AEDS3	AEDS4	FAS1	FAS2	FAS2
Sample Number	16521	16522	16523	16524	16524 D
NAG pH: (H <sub>2</sub> O <sub>2</sub> )	9.9	10.0	10.0	9.9	10.0
Titration with NaOH	0.00	0.00	0.00	0.00	0.00
Final pH: (H <sub>2</sub> O <sub>2</sub> )	9.9	10.0	10.0	9.9	10.0
NAG (kg H <sub>2</sub> SO <sub>4</sub> / t)	<0.01	<0.01	<0.01	<0.01	<0.01

Notes:

- Samples analysed with Single Addition NAG test as per Prediction Manual For Drainage Chemistry from Sulphidic Geological Materials MEND Report 1.20.1.
- Please let me know if results do not correspond to other data.

E. Botha  
Geochemistry Project Manager



WATERLAB (PTY) LTD

Building D, The Woods,
Pretoria

Telephone: +2712 - 349 - 1066
Facsimile: +2712 - 349 - 2064
Email: accounts@waterlab.co.za

CERTIFICATE OF ANALYSES
EXTRACTIONS AS 4439.3

Table with 4 columns: Date received, Project number, Report number, Date completed, Order number. Includes client name, address, and contact person details.

Main data table with columns for Analyses, Sample Number, and various chemical parameters (mg/l, ug/liter) across multiple samples (AS54 to FAS2).

[s]=subcontracted



WATERLAB (PTY) LTD

Building D, The Woods,
Pretorius Techno Park,
Maringha Road,
Pretoria

Telephone: +2712 - 349 - 1066
Facsimile: +2712 - 349 - 2064
Email: accounts@waterlab.co.za

CERTIFICATE OF ANALYSES
Digestion AS 4439.3

Date received: 23/09/2014 Date completed: 17/10/2014
Project number: 1000 Report number: 48142 Order number: ESK2840
Client name: Digby Wells Environmental Contact person: Andre van Collier
Address: Private Bag X 10046, Randburg, 2125 Email: andre.van.collier@digbywells.com
Telephone: 011 789 9495 Cell: 076 076 9443

Table with columns for Analyses, Sample Number, Digestion, Dry Mass Used (g), Volume Used (mL), Units, and various analyte results (ASS4, ASS3, ASS2, ASS1, AEDS1, AEDS2, AEDS3, AEDS4, FAS1, FAS2) and TCT0 mg/kg.

UTD = Unable to determine

(s) = subcontracted



## WATERLAB (PT)

Building D, The Woods,  
Persekor Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

### CERTIFICATE OF ANALYSES

**Date received:** 23/09/2014  
**Project number:** 1000 **Report number:** 48142

**Client name:** Digby Wells Environmental  
**Address:** Private Bag X 10046, Randburg, 2125  
**Telephone:** 011 789 9495

Analyses		
	ASS4	
Sample Number	16515	
	Liquid phase	
<b>Organics [s]</b>		
<b>VOC's: Dilution x1 - ug/liter</b>	x1	
Benzene	<2	0.01
Carbon Tetrachloride	<5	0.2
Chlorobenzene	<2	5
Chloroform	<5	15
1,2-Dichlorobenzene	<2	5
1,4-Dichlorobenzene	<2	15
1,2-Dichloroethane	<2	1.5
Ethylbenzene	<2	3.5
Hexachlorobutadiene	<2	0.03
Isopropylbenzene	<2	
MTBE	<5	2.5
Naphthalene	<2	
Styrene	<5	1
1,1,1,2-Tetrachloroethane	<10	5
1,1,2,2-Tetrachloroethane	<10	0.65
Toluene	<10	35
1,1,1-Trichloroethane	<5	15
1,1,2-Trichloroethane	<5	0.6
Xylenes total	<5	25
1,2,4 Trichlorobenzene	<2	3.5
1,2,3 Trichlorobenzene	<2	
Dichloromethane	<20	0.25
1,1-Dichloroethylene	<10	0.35
1,2-Dichloroethylene	<10	2.5
Tetrachloroethylene	<10	0.25

Trichloroethylene	<10	0.25
<b>Polars Dilution: Dilution x1 - mg/liter</b>		
2-Butanone (methyl ethyl ketone)	<50	100
Vinyl Chloride	<1	0.015
<b>Formaldehyde: Dilution x2 - ug/liter</b>		
Formaldehyde	<100	25
<b>SVOC's: Dilution x1 - ug/liter</b>		
Benzo(a)pyrene	<0.1	0.035
Di (2 ethylhexyl) Phthalate	<10	0.5
Hexachlorobenzene	<1	
Nitrobenzene	<1	1
2,4 Dinitrotoluene	<50	0.065
Hexachloroethane	<1	
Total PAH's	<2	N/A
<b>PHENOLS: Dilution x1 - ug/liter</b>		
Cresols	<2	
2-Chlorophenol	<2	15
2,4-Dichlorophenol	<2	10
Pentachlorophenol	<2	
2,4,5-Trichlorophenol	<2	
2,4,6-Trichlorophenol	<2	10
Phenols Speciated (total,non-halogenated)	<20	7
<b>Pesticides: Dilution x1 - ug/liter</b>		
Adrin	<0.1	0.015
Dieldrin	<0.1	0.015
DDT	<0.1	1
DDE	<0.1	1
DDD	<0.1	1
Heptachlor	<0.1	0.015
Chlordane	<0.1	0.05
<b>PCB: Dilution x1 - ug/liter</b>		
Ballsmitters Totals	<5	0.025
<b>TPH: Dilution x1 - ug/liter</b>		
Petroleum H/Cs,C6-C9	<10	N/A
Petroleum H/Cs,C10 to C36	UTD	N/A

UTD = Unable to determine

[s]=subcontracted

## Y) LTD

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

---

**Date completed:** 17/10/2014

**Order number:** ESK2840

---

**Contact person:** Andre van Coller

**Email:** [andre.van.coller@digbywells.com](mailto:andre.van.coller@digbywells.com)

**Cell:** 076 076 9443

---



## WATERLAB (PTY) LTD

Building D, The Woods,  
Perseus Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

### CERTIFICATE OF ANALYSES ACID – BASE ACCOUNTING EPA-600 MODIFIED SOBEK METHOD

Date received: 2014-09-23

Project number: 1000

Report number: 48142

Date completed: 2014-10-17

Order number: ESK2840

Client name: Digby Wells Environmental

Address: Private Bag X 10046, Randburg, 2125

Telephone: 011 789 9495

Facsimile: 011 789 9498

Contact person: Andre van Coller

Email:

[andre.van.coller@digbywells.com](mailto:andre.van.coller@digbywells.com)

Cell: 076 076 9443

Acid – Base Accounting Modified Sobek (EPA-600)	Sample Identification				
	ASS3	ASS2	ASS1	AEDS1	AEDS2
Sample Number	16516	16517	16518	16519	16520
Paste pH	11.1	11.3	11.4	10.9	11.1
Total Sulphur (%) (LECO)	0.15	0.17	0.19	0.17	0.22
Acid Potential (AP) (kg/t)	4.78	5.25	5.91	5.28	6.88
Neutralization Potential (NP)	42	42	42	65	70
Nett Neutralization Potential (NNP)	37	37	36	60	63
Neutralising Potential Ratio (NPR) (NP : AP)	8.7	8.0	7.1	12	10
Rock Type	III	III	III	III	III

Acid – Base Accounting Modified Sobek (EPA-600)	Sample Identification				
	AEDS3	AEDS4	FAS1	FAS2	FAS2
Sample Number	16521	16522	16523	16524	16524 D
Paste pH	11.1	11.3	12.7	12.8	12.8
Total Sulphur (%) (LECO)	0.23	0.27	0.18	0.19	0.19
Acid Potential (AP) (kg/t)	7.16	8.41	5.75	6.03	6.00
Neutralization Potential (NP)	72	77	30	49	49
Nett Neutralization Potential (NNP)	64	68	24	43	43
Neutralising Potential Ratio (NPR) (NP : AP)	10	9.1	5.2	8.1	8.2
Rock Type	III	II	III	III	III

\* Negative NP values are obtained when the volume of NaOH (0.1N) titrated (pH: 8.3) is greater than the volume of HCl (1N) to reduce the pH of the sample to 2.0 – 2.5 Any negative NP values are corrected to 0.00.

Please refer to Appendix (p.2) for a Terminology of terms and guidelines for rock classification

E. Botha  
Geochemistry Project Manager



## WATERLAB (PTY) LTD

Building D, The Woods,  
Perseus Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

### **CERTIFICATE OF ANALYSES ACID – BASE ACCOUNTING EPA-600 MODIFIED SOBEK METHOD**

Date received: 2014-09-23

Project number: 1000

Report number: 48142

Date completed: 2014-10-17

Order number: ESK2840

Client name: Digby Wells Environmental

Address: Private Bag X 10046, Randburg, 2125

Telephone: 011 789 9495

Facsimile: 011 789 9498

Contact person: Andre van Coller

Email:

[andre.van.coller@digbywells.com](mailto:andre.van.coller@digbywells.com)

Cell: 076 076 9443

#### **APPENDIX : TERMINOLOGY AND ROCK CLASSIFICATION**

##### **TERMINOLOGY (SYNONYMS)**

- Acid Potential (AP) ; *Synonyms:* Maximum Potential Acidity (MPA)  
**Method:** Total S(%) (Leco Analyzer) x 31.25
- Neutralization Potential (NP) ; *Synonyms:* Gross Neutralization Potential (GNP) ; *Syn:* Acid Neutralization Capacity (ANC) (The capacity of a sample to consume acid)  
**Method:** Fizz Test ; Acid-Base Titration (Sobek & Modified Sobek (Lawrence) Methods)
- Nett Neutralization Potential (NNP) ; *Synonyms:* Nett Acid Production Potential (NAPP)  
**Calculation:**  $NNP = NP - AP$  ;  $NAPP = ANC - MPA$
- Neutralising Potential Ratio (NPR)  
**Calculation:**  $NPR = NP : AP$

##### **CLASSIFICATION ACCORDING TO NETT NEUTRALISING POTENTIAL (NNP)**

If  $NNP (NP - AP) < 0$ , the sample has the potential to generate acid

If  $NNP (NP - AP) > 0$ , the sample has the potential to neutralise acid produced

Any sample with  $NNP < 20$  is potential acid-generating, and any sample with  $NNP > -20$  might not generate acid (Usher *et al.*, 2003)

##### **ROCK CLASSIFICATION**

<b>TYPE I</b>	Potentially Acid Forming	Total S(%) > 0.25% and NP:AP ratio 1:1 or less
<b>TYPE II</b>	Intermediate	Total S(%) > 0.25% and NP:AP ratio 1:3 or less
<b>TYPE III</b>	Non-Acid Forming	Total S(%) < 0.25% and NP:AP ratio 1:3 or greater

E. Botha

Geochemistry Project Manager



## WATERLAB (PTY) LTD

Building D, The Woods,  
Perseus Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

### CERTIFICATE OF ANALYSES ACID – BASE ACCOUNTING EPA-600 MODIFIED SOBEK METHOD

Date received: 2014-09-23

Project number: 1000

Report number: 48142

Date completed: 2014-10-17

Order number: ESK2840

Client name: Digby Wells Environmental

Address: Private Bag X 10046, Randburg, 2125

Telephone: 011 789 9495

Facsimile: 011 789 9498

Contact person: Andre van Coller

Email:

[andre.van.coller@digbywells.com](mailto:andre.van.coller@digbywells.com)

Cell: 076 076 9443

#### CLASSIFICATION ACCORDING TO NEUTRALISING POTENTIAL RATIO (NPR)

Guidelines for screening criteria based on ABA (Price *et al.*, 1997 ; Usher *et al.*, 2003)

Potential for ARD	Initial NPR Screening Criteria	Comments
Likely	< 1:1	Likely AMD generating
Possibly	1:1 – 2:1	Possibly AMD generating if NP is insufficiently reactive or is depleted at a faster rate than sulphides
Low	2:1 – 4:1	Not potentially AMD generating unless significant preferential exposure of sulphides along fracture planes, or extremely reactive sulphides in combination with insufficiently reactive NP
None	>4:1	No further AMD testing required unless materials are to be used as a source of alkalinity

#### CLASSIFICATION ACCORDING TO SULPHUR CONTENT (%S) AND NEUTRALISING POTENTIAL RATIO (NPR)

For sustainable long-term acid generation, at least 0.3% Sulphide-S is needed. Values below this can yield acidity but it is likely to be only of short-term significance. From these facts, and using the NPR values, a number of rules can be derived:

- 1) Samples with less than 0.3% Sulphide-S are regarded as having insufficient oxidisable Sulphide-S to sustain acid generation.
- 2) NPR ratios of >4:1 are considered to have enough neutralising capacity.
- 3) NPR ratios of 3:1 to 1:1 are considered inconclusive.
- 4) NPR ratios below 1:1 with Sulphide-S above 3% are potentially acid-generating. (Soregaroli & Lawrence, 1998 ; Usher *et al.*, 2003)

E. Botha  
Geochemistry Project Manager



## WATERLAB (PTY) LTD

Building D, The Woods,  
Perseus Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

### **CERTIFICATE OF ANALYSES ACID – BASE ACCOUNTING EPA-600 MODIFIED SOBEK METHOD**

---

Date received: 2014-09-23

Project number: 1000

Report number: 48142

Date completed: 2014-10-17

Order number: ESK2840

---

Client name: Digby Wells Environmental

Address: Private Bag X 10046, Randburg, 2125

Telephone: 011 789 9495

Facsimile: 011 789 9498

Contact person: Andre van Coller

Email:

[andre.van.coller@digbywells.com](mailto:andre.van.coller@digbywells.com)

Cell: 076 076 9443

---

#### **REFERENCES**

LAWRENCE, R.W. & WANG, Y. 1997. **Determination of Neutralization Potential in the Prediction of Acid Rock Drainage.** Proc. 4<sup>th</sup> International Conference on Acid Rock Drainage. Vancouver. BC. pp. 449 – 464.

PRICE, W.A., MORIN, K. & HUTT, N. 1997. **Guidelines for the prediction of Acid Rock Drainage and Metal leaching for mines in British Columbia** : Part 11. Recommended procedures for static and kinetic testing. In: Proceedings of the Fourth International Conference on Acid Rock Drainage. Vol 1. May 31 – June 6. Vancouver, BC., pp. 15 – 30.

SOBEK, A.A., SCHULLER, W.A., FREEMAN, J.R. & SMITH, R.M. 1978. **Field and laboratory methods applicable to overburdens and minesoils.** EPA-600/2-78-054. USEPA. Cincinnati. Ohio.

SOREGAROLI, B.A. & LAWRENCE, R.W. 1998. Update on waste Characterisation Studies. Proc. Mine Design, Operations and Closure Conference. Polson, Montana.

USHER, B.H., CRUYWAGEN, L-M., DE NECKER, E. & HODGSON, F.D.I. 2003. **Acid-Base : Accounting, Techniques and Evaluation (ABATE): Recommended Methods for Conducting and Interpreting Analytical Geochemical Assessments at Opencast Collieries in South Africa.** Water Research Commission Report No 1055/2/03. Pretoria.

ENVIRONMENT AUSTRALIA. 1997. **Managing Sulphidic Mine Wastes and Acid Drainage.**

E. Botha

Geochemistry Project Manager



# WATERLAB (PTY) LTD

Building D, The Woods,  
Perseus Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

## CERTIFICATE OF ANALYSES X-RAY DIFFRACTION

Date received: 2014-09-23  
Project number: 1000

Report number: 48142

Date completed: 2014-10-17  
Order number: ESK2840

Client name: Digby Wells Environmental  
Address: Private Bag X 10046, Randburg, 2125  
Telephone: 011 789 9495

Facsimile: 011 789 9498

Contact person: Andre van Collier  
Email: [andre.van.collier@digbywells.com](mailto:andre.van.collier@digbywells.com)  
Cell: 076 076 9443

Composition (%) [s]								
ASS3			ASS2			ASS1		
16516			16517			16518		
Mineral	Amount (weight %)	Error	Mineral	Amount (weight %)	Error	Mineral	Amount (weight %)	Error
Amorphous	39.33	2.31	Amorphous	34.54	2.49	Amorphous	39.75	2.4
Calcite	0.99	0.54	Calcite	1.5	0.66	Calcite	2.53	0.78
Hematite	2.02	0.45	Hematite	2.05	0.42	Hematite	1.6	0.42
Magnetite	3.77	0.33	Magnetite	3.79	0.33	Magnetite	3.1	0.33
Mullite	19.97	1.08	Mullite	22.47	1.11	Mullite	19.05	1.05
Plagioclase	18.08	1.47	Plagioclase	18.2	1.62	Plagioclase	19.29	1.53
Pyrite	0.25	0.26	Pyrite	0.41	0.2	Pyrite	0.47	0.3
Quartz	15.6	1.05	Quartz	17.03	1.11	Quartz	14.22	1.02

Composition (%) [s]								
AEDS1			AEDS2			AEDS3		
16519			16520			16521		
Mineral	Amount (weight %)	Error	Mineral	Amount (weight %)	Error	Mineral	Amount (weight %)	Error
Amorphous	36.51	2.7	Amorphous	38.06	2.52	Amorphous	35.57	2.73
Calcite	5.94	0.63	Calcite	2.45	0.45	Calcite	4.3	0.66
Hematite	0.14	0.18	Hematite	0.42	0.36	Hematite	0.38	0.33
Magnetite	2.87	0.28	Magnetite	2.55	0.3	Magnetite	2.59	0.29
Mullite	35.48	1.74	Mullite	34.49	1.8	Mullite	36.13	1.83
Plagioclase	2.7	1.56	Plagioclase	1.45	0.84	Plagioclase	3.79	1.29
Pyrite	0.32	0.18	Pyrite	0.76	0.3	Pyrite	0.6	0.29
Quartz	16.04	1.11	Quartz	19.83	1.17	Quartz	16.65	1.08

The information contained in this report is relevant only to the sample/samples supplied to **WATERLAB (Pty) Ltd**. Any further use of the above information is not the responsibility or liability of **WATERLAB (Pty) Ltd**. Except for the full report, parts of this report may not be reproduced without written approval of **WATERLAB (Pty) Ltd**.



## WATERLAB (PTY) LTD

Building D, The Woods,  
Perseus Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

### CERTIFICATE OF ANALYSES X-RAY DIFFRACTION

Date received: 2014-09-23  
Project number: 1000

Report number: 48142

Date completed: 2014-10-17  
Order number: ESK2840

Client name: Digby Wells Environmental  
Address: Private Bag X 10046, Randburg, 2125  
Telephone: 011 789 9495

Facsimile: 011 789 9498

Contact person: Andre van Collier  
Email: [andre.van.collier@digbywells.com](mailto:andre.van.collier@digbywells.com)  
Cell: 076 076 9443

Composition (%) [s]								
AEDS4			FAS1			FAS2		
16522			16523			16524		
Mineral	Amount (weight %)	Error	Mineral	Amount (weight %)	Error	Mineral	Amount (weight %)	Error
Amorphous	37.9	2.73	Amorphous	37.14	2.55	Amorphous	39.86	2.25
Calcite	3.95	0.69	Lime	2.18	0.25	Lime	1.96	0.24
Hematite	0.45	0.36	Calcite	0.63	0.48	Calcite	0	0
Magnetite	2.62	0.3	Hematite	0.92	0.39	Hematite	0.92	0.36
Mullite	32.64	1.83	Magnetite	3.55	0.33	Magnetite	3.48	0.3
Plagioclase	3.17	1.26	Mullite	34.05	1.74	Mullite	35.4	1.74
Pyrite	0.57	0.3	Plagioclase	1.78	0.9	Plagioclase	0	0
Quartz	18.7	1.14	Pyrite	0.54	0.33	Pyrite	0.41	0.29
			Quartz	19.22	1.23	Quartz	17.97	1.14

[s] Results obtained from sub-contracted laboratory

**Note:**

The material submitted was scanned after addition of 20 % Si for quantitative determination of amorphous content and homogenizing using a McCrone micronizing mill. The material was prepared for XRD analysis using a backloading preparation method. It was analysed with a PANalytical Empyrean diffractometer with PIXcel detector and fixed slits with Fe filtered Co-K $\alpha$  radiation. The phases were identified using X'Pert Highscore plus software.

The relative phase amounts (weight%) were estimated using the Rietveld method. Mathematical errors of the method are shown at the right hand side of the amounts.

**Comment:**

- Due to crystallite size effects results errors may be larger than shown.
- In case the results do not correspond to results of other analytical techniques, please let me know for further fine tuning of XRD results.
- Results are also attached as excel file.
- Mineral names may not reflect the actual compositions of minerals identified, but rather the mineral group.



## WATERLAB (PTY) LTD

Building D, The Woods,  
Perseus Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

### CERTIFICATE OF ANALYSES X-RAY DIFFRACTION

---

Date received: 2014-09-23  
Project number: 1000

Report number: 48142

Date completed: 2014-10-17  
Order number: ESK2840

---

Client name: Digby Wells Environmental  
Address: Private Bag X 10046, Randburg, 2125  
Telephone: 011 789 9495

Facsimile: 011 789 9498

Contact person: Andre van Coller  
Email: [andre.van.coller@digbywells.com](mailto:andre.van.coller@digbywells.com)  
Cell: 076 076 9443

---

---

#### Ideal Mineral Formula

Quartz	Si O <sub>2</sub>
Plagioclase	( Na , Ca ) Al ( Si , Al ) <sub>3</sub> O <sub>8</sub>
Lime	CaO
Magnetite	Fe <sub>3</sub> O <sub>4</sub>
Pyrite	Fe S <sub>2</sub>
Calcite	CaCO <sub>3</sub>
Mullite	Al <sub>4,5</sub> Si <sub>1,5</sub> O <sub>9,75</sub>
Hematite	Fe <sub>2</sub> O <sub>3</sub>

---



**WATERLAB**

**WATERLAB (PTY) LTD**

Building D, The Woods,  
Perseus Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

**CERTIFICATE OF ANALYSES  
X-RAY FLUORESCENCE**

Date received: 2014-09-23  
Project number: 1000

Report number: 48142

Date completed: 2014-10-17  
Order number: ESK2840

Client name: Digby Wells Environmental  
Address: Private Bag X 10046, Randburg, 2125  
Telephone: 011 789 9495

Facsimile: 011 789 9498

Contact person: Andre van Coller  
Email: [andre.van.coller@digbywells.com](mailto:andre.van.coller@digbywells.com)  
Cell: 076 076 9443

Major Elements	Major Element Concentration (wt %)[s]								
	ASS3	ASS2	ASS1	AEDS1	AEDS2	AEDS3	AEDS4	FAS1	FAS2
	16516	16517	16518	16519	16520	16521	16522	16523	16524
SiO <sub>2</sub>	49.28	48.99	51.81	47.95	50.34	47.48	48.16	51.38	50.53
TiO <sub>2</sub>	1.51	1.5	1.52	1.68	1.6	1.61	1.61	1.730	1.700
Al <sub>2</sub> O <sub>3</sub>	27.97	28.39	28.58	30.34	29.99	30.54	29.30	30.82	30.66
Fe <sub>2</sub> O <sub>3</sub>	4.06	3.66	3.92	2.49	2.34	2.43	2.67	2.85	2.650
MnO	0.04	0.04	0.05	0.03	0.03	0.03	0.04	0.03	0.03
MgO	1.27	1.24	1.34	1.4	1.3	1.44	1.35	0.94	0.89
CaO	9.47	9.06	9.57	6.82	6.16	6.99	7.69	7.09	6.82
Na <sub>2</sub> O	0.07	0.05	0.03	0.21	0.18	0.34	0.19	0.12	0.15
K <sub>2</sub> O	0.72	0.73	0.72	0.86	0.87	0.81	0.93	0.68	0.66
P <sub>2</sub> O <sub>5</sub>	0.4	0.39	0.43	0.72	0.59	0.69	0.64	0.56	0.54
Cr <sub>2</sub> O <sub>3</sub>	0.02	0.02	0.02	0.02	0.02	0.04	0.02	0.02	0.02
SO <sub>3</sub>	0.85	0.77	0.6	0.6	0.82	0.830	0.990	0.830	0.830
LOI	2.28	2.52	2.04	7.26	6.11	5.11	6.32	1.7	1.17
Total	98.43	97.36	100.63	100.38	100.35	98.34	99.91	98.75	96.65
H <sub>2</sub> O-	0.49	0.53	0.31	1.07	2.07	0.76	1.64	0.10	0.16

[s] = Results obtained from sub-contracted laboratory

**Notes:** % g/g is equivalent to wt %; mg/kg is equivalent to ppm; n.d. = not determined; bold italicised font represents semi-quantitative data; \* represents measurements reported in % g/g or wt%.

E. Botha  
Geochemistry Project Manager

The information contained in this report is relevant only to the sample/samples supplied to WATERLAB (Pty) Ltd. Any further use of the above information is not the responsibility or liability of WATERLAB (Pty) Ltd. Except for the full report, parts of this report may not be reproduced without written approval of WATERLAB (Pty) Ltd.



# WATERLAB (PTY) LTD

Building D, The Woods,  
Perseus Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

## CERTIFICATE OF ANALYSES X-RAY FLUORESCENCE

Date received: 2014-09-23  
Project number: 1000

Report number: 48142

Date completed: 2014-10-17  
Order number: ESK2840

Client name: Digby Wells Environmental  
Address: Private Bag X 10046, Randburg, 2125  
Telephone: 011 789 9495

Facsimile: 011 789 9498

Contact person: Andre van Coller  
Email: [andre.van.coller@digbywells.com](mailto:andre.van.coller@digbywells.com)  
Cell: 076 076 9443

Trace Elements	Trace Element Concentration (ppm) [s]								
	ASS3	ASS2	ASS1	AEDS1	AEDS2	AEDS3	AEDS4	FAS1	FAS2
	16516	16517	16518	16519	16520	16521	16522	16523	16524
As	1.55	4.33	2.47	15.2	16.3	16.40	15.90	11.30	11.70
Ba	814	798	745	954	932	966.00	1021.00	710.00	729.00
Bi	1.3	1.43	0.9	1.56	1.68	1.84	1.36	1.23	1.4
Cd	4.42	5.03	4.78	4.94	3.55	6.85	5.87	4.98	4.62
Ce	187	127	73.9	108	129	101.00	101.00	131.00	117.00
Cl	117	129	122	141	132	99	106	94.6	90.8
Co	<0.56	<0.56	<0.56	<0.56	<0.56	<0.56	<0.56	<0.56	<0.56
Cs	2.18	3.8	3.85	4.69	1.85	4.21	7.78	3.2	3.55
Cu	44.8	44	38.2	59.4	58.9	62	57.7	52.6	54
Ga	24.5	24	21.4	45.6	39.8	40.4	40.1	35.3	36
Ge	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50
Hf	7.37	11.1	3.37	1.92	1.71	6.39	2.95	2.36	6.46
Hg	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00
La	23.1	61.1	42.9	34	44.8	39.9	37.6	62	33.4
Lu	2.58	2.47	2.37	2.17	2.15	2.25	2.22	2.29	2.27
Mo	2.35	2.31	2.35	2.28	2.23	2.3	2.27	2.26	2.25
Nb	32.9	36.4	31.5	41.3	39.2	40.2	40.8	37.8	37.3
Nd	<2.39	<2.39	<2.39	35.6	44	58	46.4	<2.39	<2.39
Ni	39.1	34.8	34.2	51	45.5	53.2	39.4	54.2	46.2
Pb	<2.03	<2.03	<2.03	100	101	111	91	68.6	71.4
Rb	32.7	35.7	29.9	55.5	53	50.8	57.7	38.4	39.1
Sb	4.63	<1.48	<1.48	4.4	4.64	2.66	<1.48	<1.48	2.79
Sc	35	43.2	38.3	33.5	31.4	33.3	35.8	31.2	34
Se	3.02	2.24	2.87	8.99	7.36	8.58	6.86	5.51	6.07
Sm	14.5	14.9	14.1	3.37	7.26	4.38	6.11	8.18	10.5
Sn	18.5	14.5	12.5	18.5	18.4	17.5	19.5	15.5	14.5
Sr	1 908	1 893	1 723	2 569	1 928	2 388	2 340	1 595	1 607
Ta	1.21	1.54	1.82	1.43	1.35	1.61	1.62	2.19	1.76
Te	21.6	17	18.8	17.4	11.4	13.2	16.1	18.4	15.1
Th	25.6	24.7	25.6	33.3	29	30.3	32.3	32.3	30.9
Tl	0.71	0.65	0.37	1.06	0.78	0.95	1.25	0.87	0.84

Results continued on next page

E. Botha  
Geochemistry Project Manager

The information contained in this report is relevant only to the sample/samples supplied to WATERLAB (Pty) Ltd. Any further use of the above information is not the responsibility or liability of WATERLAB (Pty) Ltd. Except for the full report, parts of this report may not be reproduced without written approval of WATERLAB (Pty) Ltd.



## WATERLAB (PTY) LTD

Building D, The Woods,  
Persekor Techno Park,  
Meiring Naudé Road, Pretoria  
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066  
Facsimile: +2712 – 349 – 2064  
Email: [accounts@waterlab.co.za](mailto:accounts@waterlab.co.za)

### CERTIFICATE OF ANALYSES X-RAY FLUORESCENCE

Date received: 2014-09-23  
Project number: 1000

Report number: 48142

Date completed: 2014-10-17  
Order number: ESK2840

Client name: Digby Wells Environmental  
Address: Private Bag X 10046, Randburg, 2125  
Telephone: 011 789 9495

Facsimile: 011 789 9498

Contact person: Andre van Coller  
Email: [andre.van.coller@digbywells.com](mailto:andre.van.coller@digbywells.com)  
Cell: 076 076 9443

Trace Elements	Trace Element Concentration (ppm) [s]								
	ASS3	ASS2	ASS1	AEDS1	AEDS2	AEDS3	AEDS4	FAS1	FAS2
	16516	16517	16518	16519	16520	16521	16522	16523	16524
U	14.9	13.6	13.2	23.1	15.3	20.3	18.2	13.8	13.9
V	<7.60	<7.60	<7.60	<7.60	<7.60	<7.60	<7.60	<7.60	<7.60
W	1.33	1.32	1.26	1.18	1.16	1.16	1.3	1.13	1.22
Y	67.3	68.2	61.5	80.6	74.4	76.4	79.5	70.3	71.2
Yb	10.1	10.1	7.34	5.81	4.84	6.8	7.28	3.77	8.88
Zn	32	30.8	30.9	55.3	52.3	50.8	47.5	46.6	43.5
Zr	479	483	444	535	478	518	521	473	479

[s] = Results obtained from sub-contracted laboratory

#### XRF: Major Element Analysis (Geological)

The samples were prepared by first drying the samples at 100°C for ~3 hours in order to determine loss of moisture content (H<sub>2</sub>O-), followed by ashing of the sample at 1000°C until completely ashed, to determine the loss on ignition (LOI). XRF analyses were performed using a PANalytical Epsilon 3 XL ED-XRF spectrometer, equipped with a 50kV Ag-anode X-ray tube, 6 filters, a helium purge facility and a high resolution silicon drift detector, calibrated using a number of international and national certified reference materials (CRMs).

#### XRF: Trace Element Analysis (Geological)

XRF analyses were performed using a PANalytical Epsilon 3 XL ED-XRF spectrometer, equipped with a 50kV Ag-anode X-ray tube, 6 filters, a helium purge facility and a high resolution silicon drift detector, calibrated using international and national certified reference materials (CRMs).

E. Botha  
Geochemistry Project Manager

The information contained in this report is relevant only to the sample/samples supplied to **WATERLAB (Pty) Ltd**. Any further use of the above information is not the responsibility or liability of **WATERLAB (Pty) Ltd**. Except for the full report, parts of this report may not be reproduced without written approval of **WATERLAB (Pty) Ltd**.